

# Effect of Tape Inhomogeneity on the Critical Current Estimation of HTS Coil



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## INTRODUCTION

The commercially available HTS tapes like  $\text{REBa}_2\text{Cu}_3\text{O}_x$  (where RE = Rare Earth) tape always present a certain critical current ( $I_c$ ) inhomogeneity along the tape due to manufacturing defects and process variations. It is necessary to take into consideration the  $I_c$  inhomogeneity of tape for an accurate estimate on the  $I_c$  of HTS devices. There are various characterizations on the tape's  $I_c$  inhomogeneity. From the detailed  $I_c$  data, one can characterize the tape's  $I_c$  inhomogeneity with the maximal  $I_c$ , minimal  $I_c$ , mean  $I_c$  and the so-called overall  $I_c$ .

This work is to estimate the  $I_c$  of several HTS DP coils in consideration of the varied characterizations and two different criteria, i.e., MAX and AVG criteria. Through a comprehensive comparison on the coil  $I_c$  between the calculation and measurement, a few appropriate characterizations on the inhomogeneity are determined for estimating the  $I_c$  of HTS coils during their design and operation stages. This study can provide useful implications for the design of HTS coils that are wound by the tapes with noteworthy  $I_c$  inhomogeneity.

## SIMULATION AND EXPERIMENT

### I. Characterizations of Tape's $I_c$ Inhomogeneity

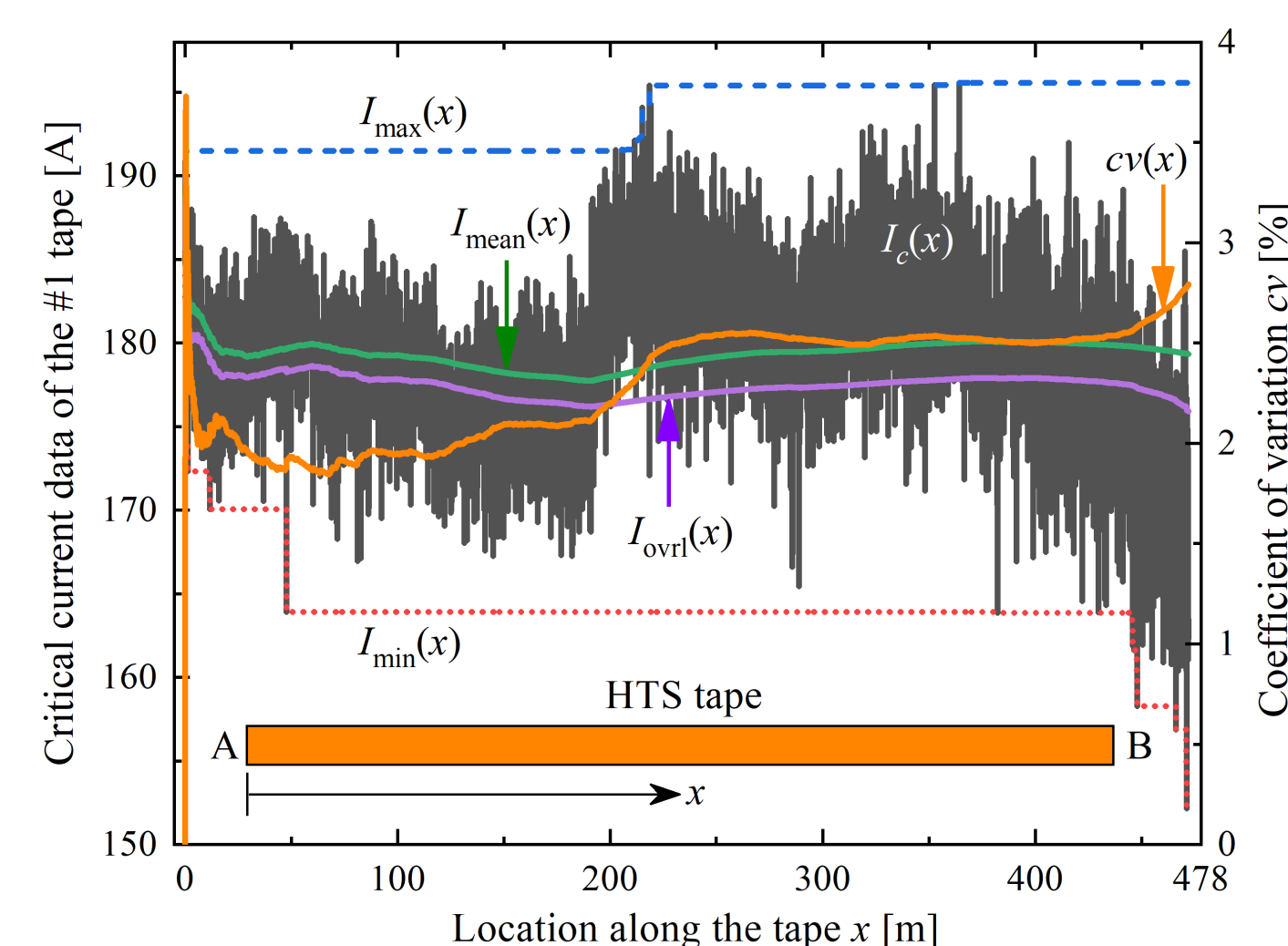


Fig. 1. Characterizations on tape's  $I_c$  inhomogeneity.

It is clearly evident that  $I_{\max}(x) > I_{\text{mean}}(x) > I_{\text{ovrl}}(x) > I_{\min}(x)$  and  $I_{\text{ovrl}}(x) \approx I_{\text{mean}}(x)$ . The  $I_{\max}(x)$  and  $I_{\min}(x)$  monotonically change with the location  $x$ . However, the  $I_{\text{mean}}(x)$  and  $I_{\text{ovrl}}(x)$  are not monotonous because of the inhomogeneity, which are able to better characterize the tape's  $I_c$  inhomogeneity.

### II. Homogenized Self-Consistent Mode

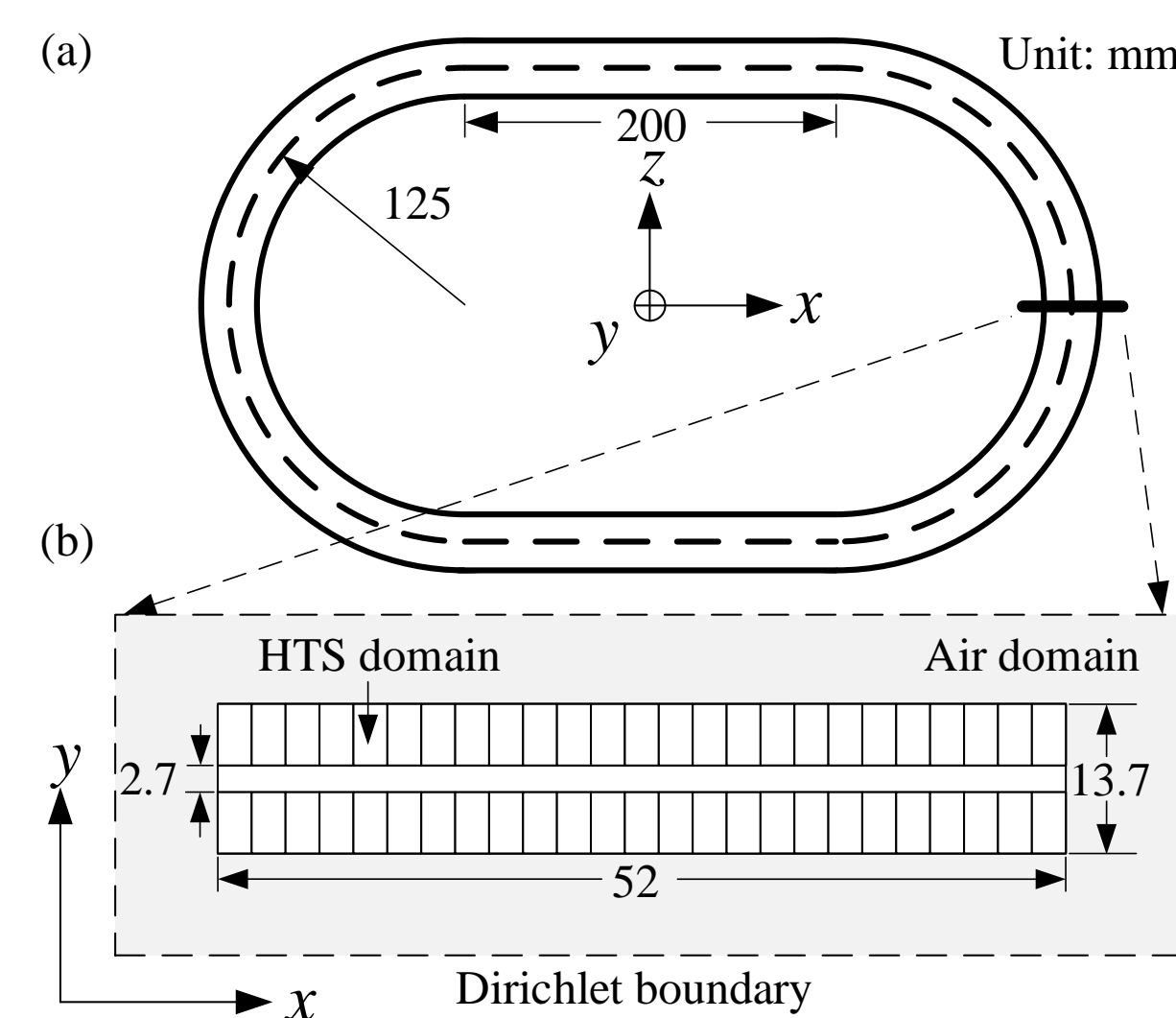


Fig. 2. Geometric layout (a) and the homogenized self-consistent model (b) of the HTS DP coil.

The self-field of the racetrack HTS double-pancake (DP) coil, obtained by resorting to a numerical model, is applied as Dirichlet boundary condition on the outer boundary of this model including only the HTS domain and a thin air domain.

### III. Manufacture and measurement

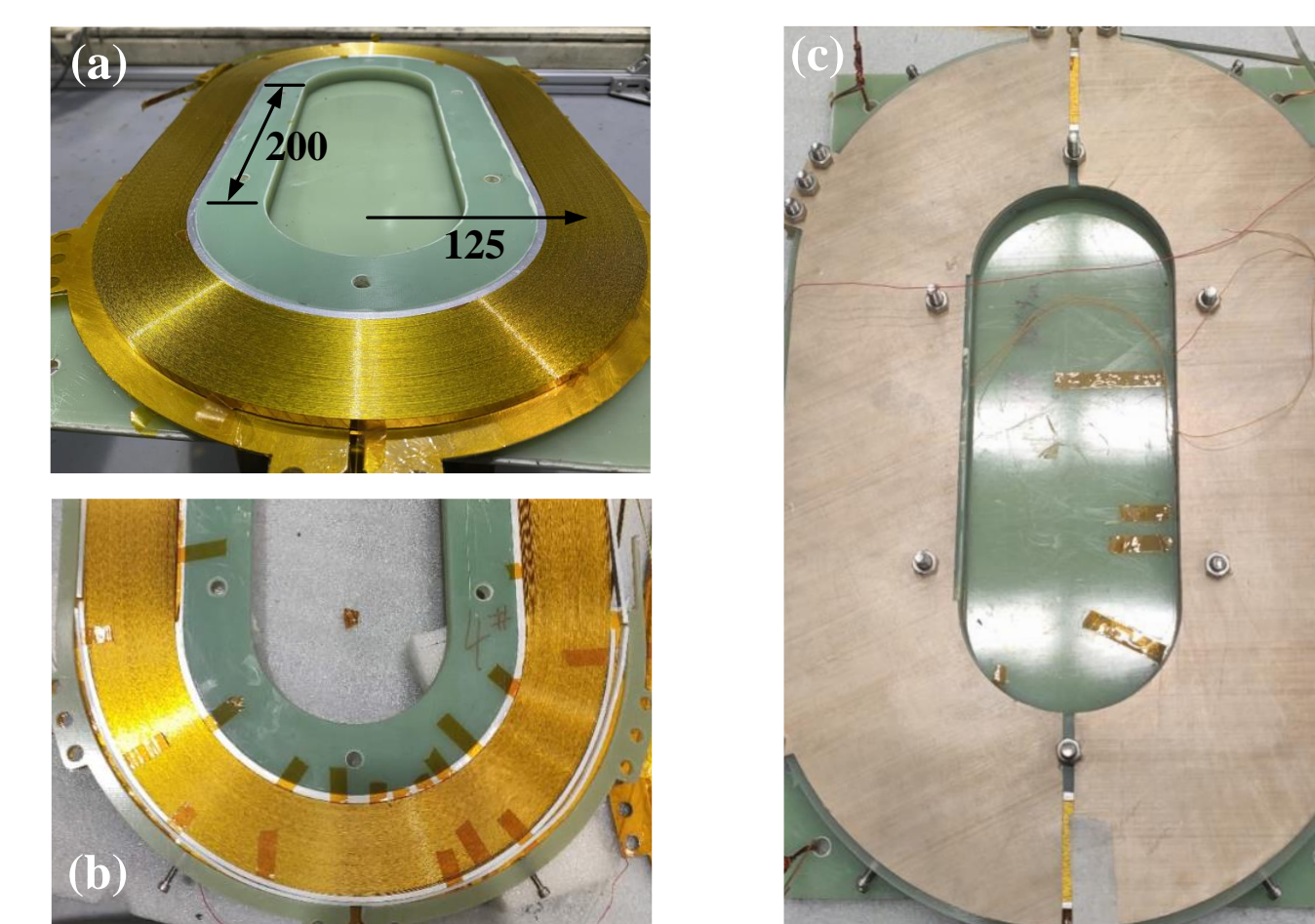


Fig. 3. Manufacture of the racetrack HTS DP coil, (a) the winding of DP coil, (b) the coil fastening, and (c) one fabricated DP coil.

With the HTS tapes described in Fig. 1, four racetrack HTS DP coils were fabricated and their critical currents were measured at liquid nitrogen temperature.

## RESULTS AND DISCUSSION

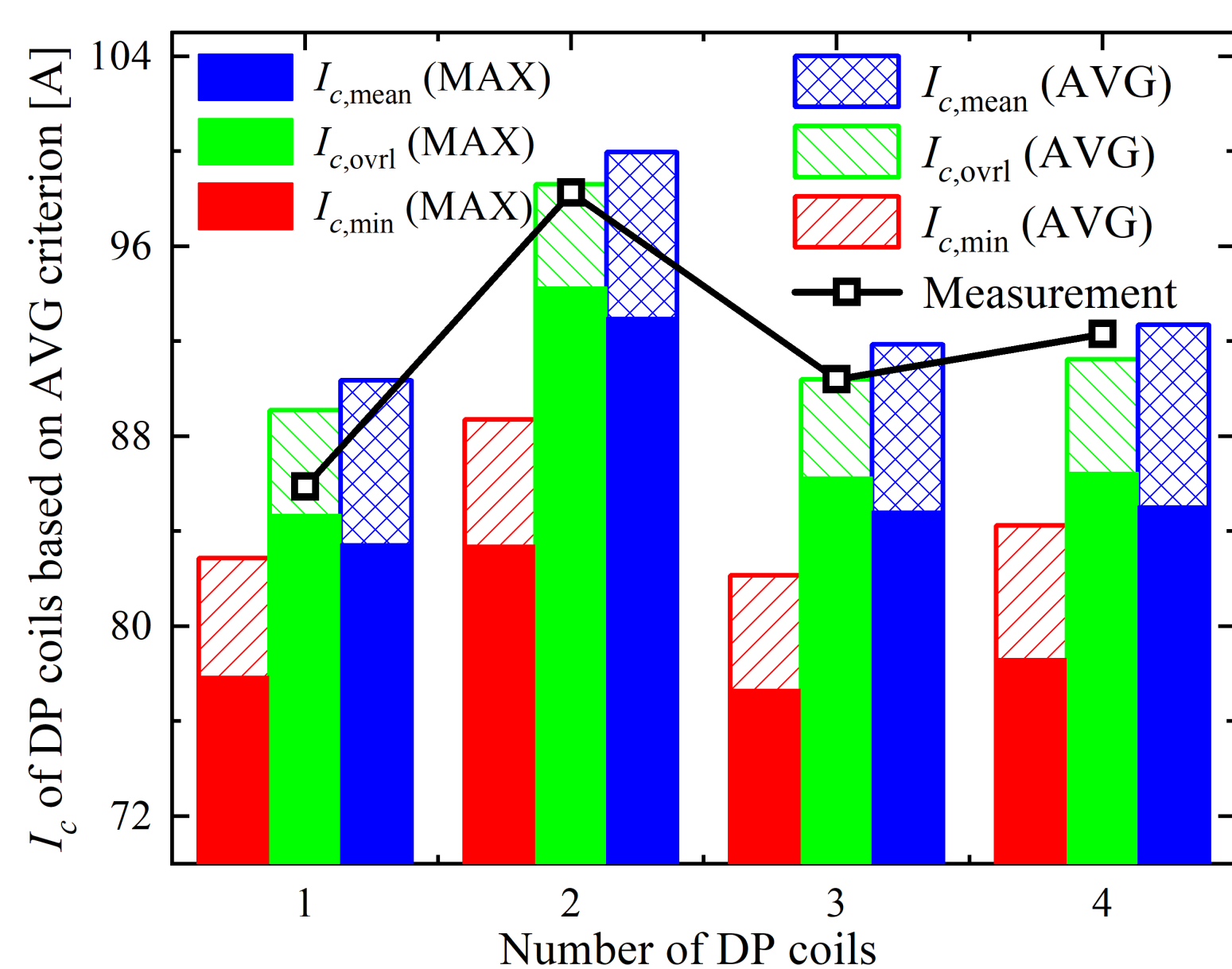


Fig. 4. Comparison of  $I_c$  of the four HTS DP coils from the measurement and calculation.

- ✓  $I_c$  of all DP coils meet  $I_{c,\text{mean}} > I_{c,\text{ovrl}} > I_{c,\text{min}}$ ;
- ✓  $I_c$  (AVG) is higher than the one (MAX);
- ✓  $I_{c,\text{ovrl}}$  (AVG) is closest to the measured one;
- ✓ all the calculated  $I_c$  (MAX) are below the measured values;
- ✓ the measured  $I_c$  are within the certain range of  $I_{c,\text{min}}$  (MAX) and  $I_{c,\text{mean}}$  (AVG).

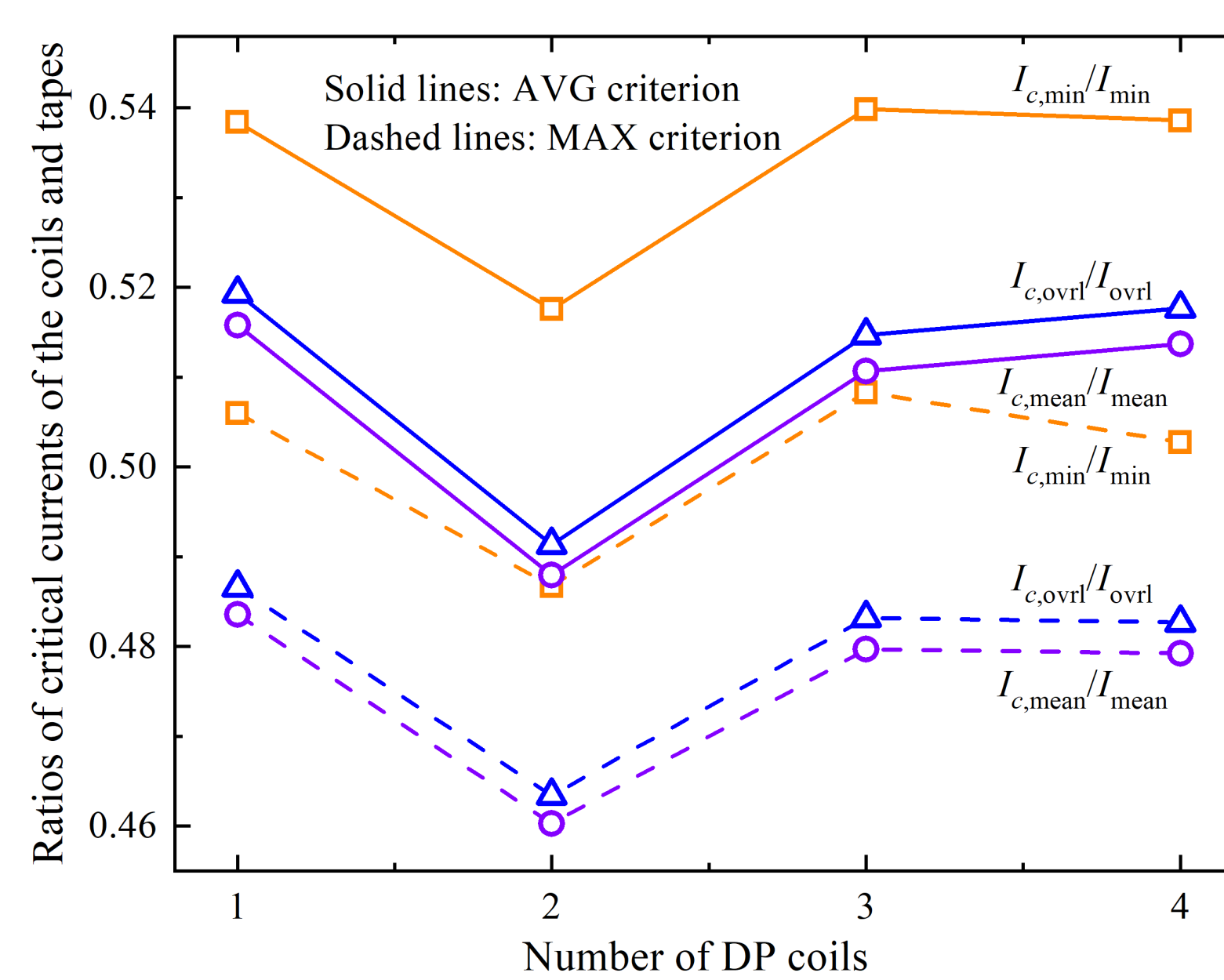


Fig. 5. Ratios of the  $I_c$  of the four HTS DP coils to the corresponding tapes.

- ✓ The attenuation factor is about 0.5 after these tapes are wound into DP coils;
- ✓ The ratio of  $I_c$  of coil to tape little depends on the inhomogeneity and the selected criterion;
- ✓ As for the MAX and AVG criteria, the latter gives a greater ratio;
- ✓  $I_c$  of a DP coil can be estimated by the ratio of the  $I_c$  between these tapes.

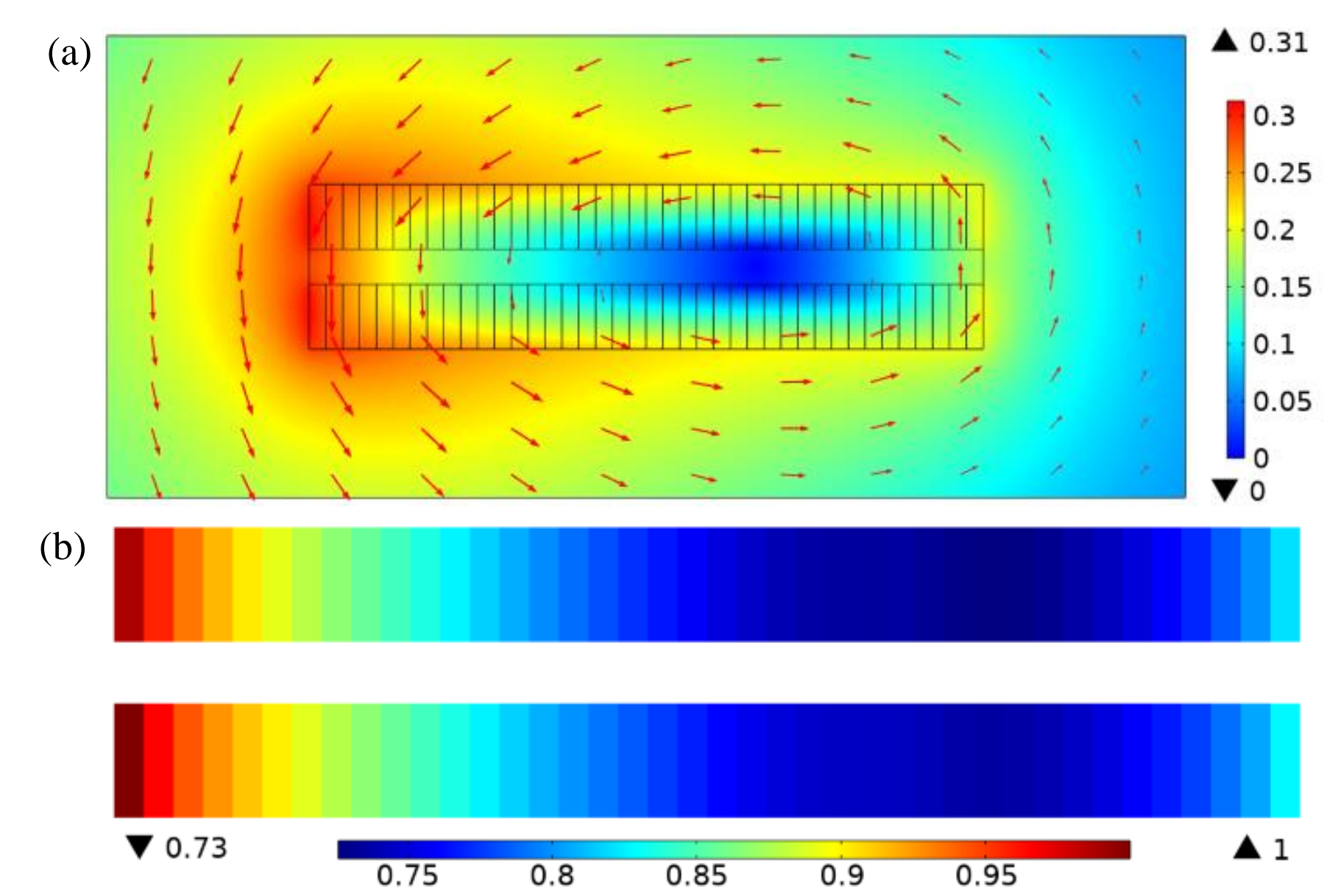


Fig. 6. Distribution of (a) the magnetic flux density (unit: T) and (b) load factor in the DP4 for the case of the tape's  $I_{\min}$  and MAX criterion.

- ✓ The magnetic flux density mostly concentrates on the inner of coil, giving rise to the highest load factor. This finding implies that the inner turns of the coil should be wound with the tape section having a higher  $I_c$ .

## CONCLUSIONS

1. With the tape's  $I_c$  inhomogeneity considered, the  $I_c$  of four HTS DP coils was estimated by means of a homogenized self-consistent model. Detailed comparison and discussion on the  $I_c$  of the calculation and measurement were conducted.
2. The  $I_c$  of a HTS coil can be better estimated in consideration of the  $I_{\text{ovrl}}$  of tape and AVG criterion. By contrast, the  $I_{\text{mean}}$  of tape and MAX criterion are a better combination for obtaining a conservative estimate on the  $I_c$  of a HTS coil during the design stage. Normally, the measured critical current of a HTS coil must be within the certain range of  $I_{c,\text{min}}$  (MAX) and  $I_{c,\text{mean}}$  (AVG).
3. The ratio of the  $I_c$  of these DP coils to their tapes little depends on the  $I_c$ -inhomogeneity characterization and the selected criterion.