

The CEA logo consists of the lowercase letters 'cea' in a white, sans-serif font, positioned above a thin horizontal green line. The logo is centered within a dark red square background.The IRFM logo features the lowercase letters 'irfm' in a white, cursive-style font. A yellow and green circular graphic element is positioned to the left of the text. The logo is centered within a dark red square background.

The benefits of the analytical approach for the optimization of superconducting magnets from the early design stage

| *Young Scientist Plenary MT27 Conference, November 17th 2021*

Alexandre LOUZGUITI, CEA IRFM, EUROfusion Engineering Grant

■ Superconducting magnet

- Multiphysics
- Multifunction
- Different sizes & environments



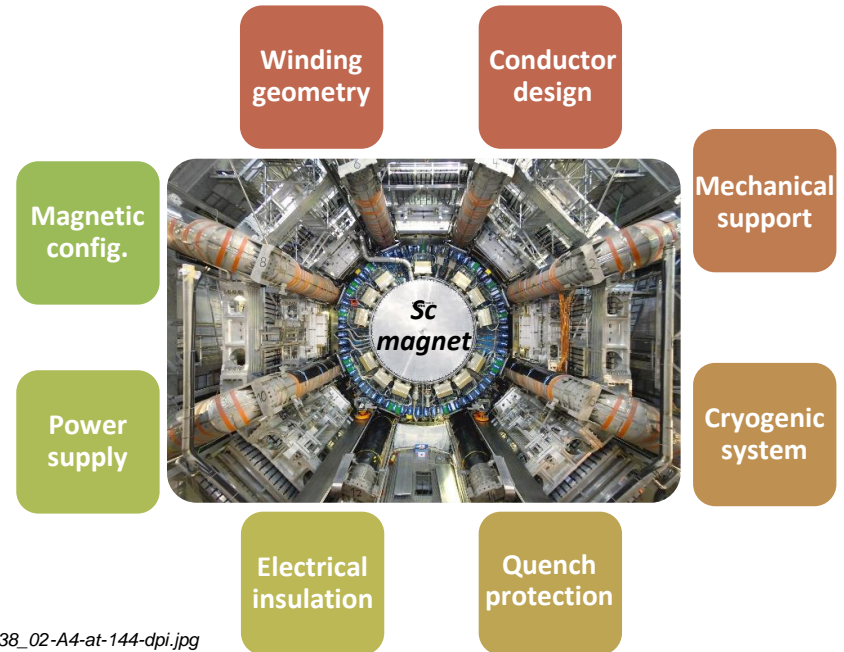
complex object

■ Difficult to design since it requires different

- experts
- technologies
- design tools

■ To reduce complexity of design process

- Predesign phase is often limited to winding geometry definition from magnetic configuration requirements
- The other systems are then usually treated more sequentially in the conceptual design phase

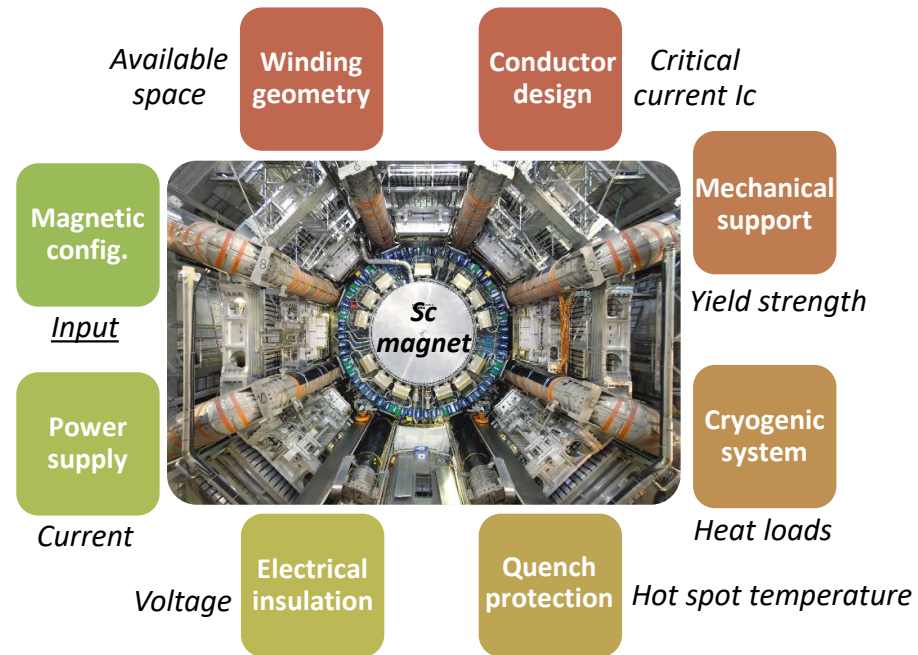


■ During predesign, a more global approach including different systems will lead to a more optimized magnet in terms of cost and performance

■ Such an approach is difficult to formulate and to interface between experts/tools

■ An analytical approach at this stage allows to

- account for the *limiting effects* of different systems in parallel in a simplified yet **realistic/conservative** and **rapid** way
- derive scaling laws of the magnet properties with respect to its parameters (e.g. peak field vs winding thickness)



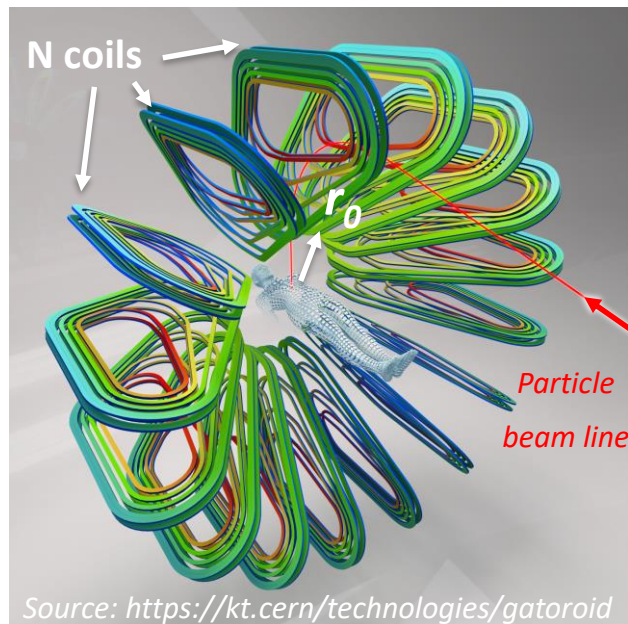
■ **GaToroid^{1,2} = Toroidal gantry for hadrontherapy**

- N coils \rightarrow number of treatment angles
- Aperture $r_0 \rightarrow$ free bore for patient

■ **Stored energy E** is a good indicator of magnet **cost and complexity** as it contains the information of forces and needs to be extracted by the quench protection system

- Computed through $\iiint_{space} \frac{B^2}{2\mu_0} dV$ (magnetic configuration) or $\frac{1}{2} LI^2$ (winding geometry)
- Needs to be **minimized** to reduce cost & complexity

■ **Question** : how does E scale with N and r_0 ?



¹L. Bottura, A Gantry and Apparatus for Focusing Beams of Charged Particles, [European Patent Application EP 18173426.0](#), May 2018

²L. Bottura, E. Felcini, G. De Rijck, B. Dutoit, "GaToroid: A Novel Toroidal Gantry for Hadron Therapy", Nucl. Instrum. Methods Phys. Res. A, 2020

- 3D geometry **too complex**, so stored energy **E analytical** formula derived from **simplified** 2D approach in toroidal plane

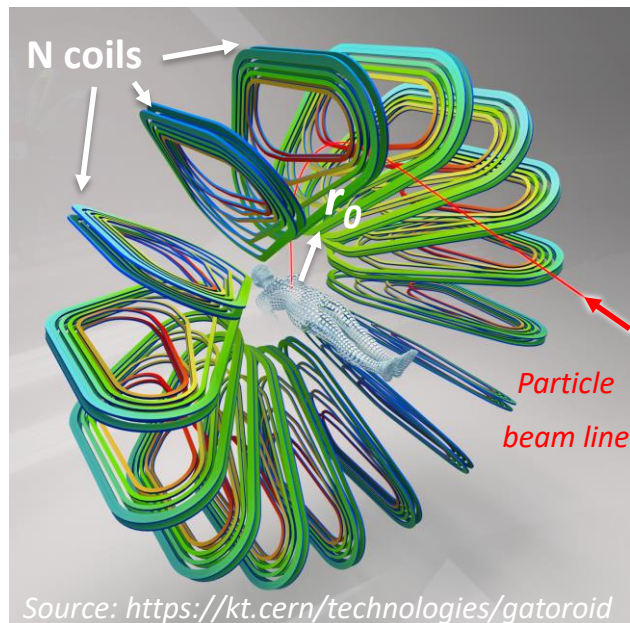
$$E = \frac{\mu_0(2NI_0)^2 h}{4\pi} \left[\ln\left(\frac{r_2}{r_1}\right) - \frac{2\ln(2N)}{2N} + \frac{1}{2N} \ln\left(\frac{r_1 r_2}{r_c^2}\right) + \frac{2\ln(2) - \ln\left(1 - \cos\left(\frac{2Nd}{r_1}\right)\right) - \ln\left(1 - \cos\left(\frac{2Nd}{r_2}\right)\right)}{4N} \right]$$

with $r_1 = r_0 + r_c + 0.15 \text{ m}$, $r_2 = r_1 - 2r_c + 2.296 \text{ m}$, $d = 0.137 \text{ m}$, $r_c = 0.128 \text{ m}$, $h = 1.75 \text{ m}$

- Answer to **E scaling with N and r_0** :

		Analytical formula			Numerical code			
		$r_0 = 1.5\text{m}$	$r_0 = 1.65\text{m}$	$r_0 = 2\text{m}$	$r_0 = 1.5\text{m}$	$r_0 = 1.65\text{m}$	$r_0 = 2\text{m}$	
E scaling	$N = 16$	0,92	1,03	1,27	$N = 16$	0,90	1,01	1,26
	$N = 20$	0,90	1,00	1,22	$N = 20$	0,89	1,00	1,24
	$N = 24$	0,90	0,99	1,20	$N = 24$	0,89	0,99	1,23

- **E scaling law vs N and r_0 derived from the simplified analytical formula agrees well with numerical results !**



■ **Global analytical approach** to account for *limiting effects* of each system and **optimize the magnet design**

■ **Winding geometry**

- Stored magnetic energy: $E = \frac{1}{2}LI^2$

■ **Conductor design**

- Stability: $J_{sc} = J_c(B_p, T_{op} + \Delta T_m)$
- Geometry: $CuSc = \frac{A_{cu}}{A_{sc}}, f = \frac{A_{cu} + A_{sc}}{A_{cond}} = \frac{3}{4}$
- Current: $I = J_0 A_{cond} = J_{sc} A_{sc} = J_{cu} A_{cu}$
- Physical properties: $\mu C_p = \frac{f}{1 + CuSc} (CuSc \mu_{cu} C_{p,cu} + \mu_{sc} C_{p,sc}), \rho = \frac{1 + CuSc}{f CuSc} \rho_{cu}$

$$J_0 = \frac{f J_c(B_p, T_{op} + \Delta T_m)}{1 + CuSc} : (1)$$

$$E = 540 \text{ MJ}, B_p = 8.21 \text{ T}$$

■ **Quench protection system**

- Discharge on dump R_d time constant: $\tau = L/R_d$
- Max voltage: $U = R_d I$
- MIITs: $\int J_0^2 dt = \frac{\tau}{2} J_0^2 = \int_{T_{op}}^{T_h} \frac{\mu C_p}{\rho} dT : (2)$

$$(1) \ \& \ (2): \ CuSc^2 \int_{T_{op}}^{T_h} \frac{\mu_{cu} C_{p,cu}}{\rho_{cu}} dT + CuSc \int_{T_{op}}^{T_h} \frac{\mu_{sc} C_{p,sc}}{\rho_{cu}} dT - \frac{E}{U_d I} J_c^2(B_p, T_{op} + \Delta T_m) = 0 \quad U = 1 \text{ kV}$$

Available
space

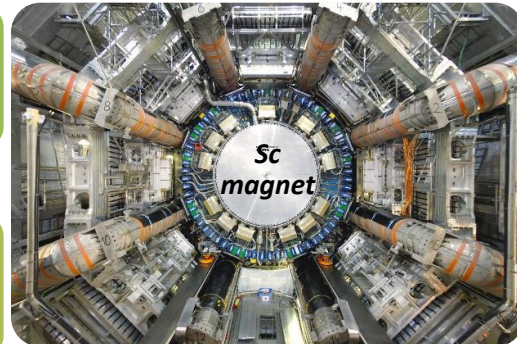
Winding
geometry

Conductor
design

Nb-Ti

$$\Delta T_m = T_{cs} - T_{op} = 1 \text{ K}$$

Magnetic
config.



Mechanical
support

Yield strength

Cryogenic
system

Heat loads
 $T_{op} = 4.2 \text{ K}$

Adiabatic $T_h = 150 \text{ K}$

Common dump resistor

Power
supply

$I = 12 \text{ kA}$

Electrical
insulation

Quench
protection

- Global analytical approach to account for limiting effects of each system and optimize magnet

$$CuSc^2 \int_{T_{op}}^{T_h} \frac{\mu_{cu} C_{p,cu}}{\rho_{cu}} dT + CuSc \int_{T_{op}}^{T_h} \frac{\mu_{sc} C_{p,sc}}{\rho_{cu}} dT - \frac{E}{U_d I} J_c^2 (B_p, T_{op} + \Delta T_m) = 0$$

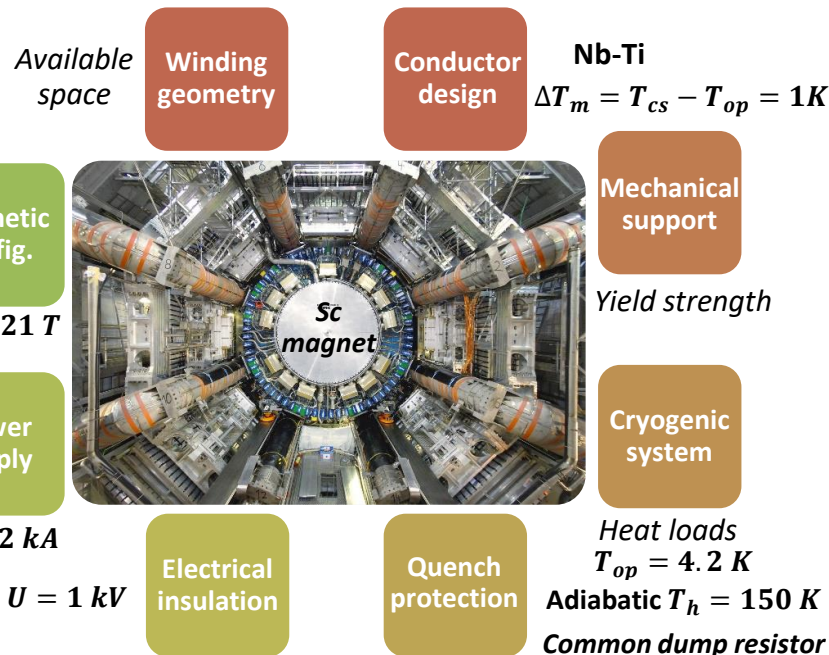
$$\text{Solution: } \alpha CuSc^2 + \beta CuSc - \gamma = 0 \rightarrow CuSc = \sqrt{\left(\frac{\beta}{2\alpha}\right)^2 + \frac{\gamma}{\alpha}} - \frac{\beta}{2\alpha}$$

- Parameters ensuring that all systems are fulfilling the defined criteria:

- Copper to superconducting ratio $CuSc = 7.87$
- Engineering current density $J_0 = 29 \text{ A/mm}^2$
- Conductor area $A_{cond} = 414 \text{ mm}^2$
- Discharge time constant $\tau = 90 \text{ s}$

→ Magnet is optimized at predesign stage

- Exercise can be repeated with different conditions and different quench protection systems (e.g. quench heaters)



- This global **analytical** approach allows to **optimize** the **magnet from the predesign** stage → the optimization can be further refined locally with numerical/FEM models during the conceptual design phase

- This **analytical baseline** is interesting to **formulate** and to **integrate from** the **predesign** phase in a **sc magnet project** as it can also be the **embryo** of:
 - **System codes** such as SYCOMORE or PROCESS if combined with a **numerical platform**
 - **A tool to rapidly control** the impact of deviations from design specifications on the magnet future operation if combined with an **updated parameters database along magnet manufacturing and quality controls** (e.g. Jc fit impact on Tcs, RRR impact on hot spot, etc.)
 - **A fast and light modeling tool** during **magnet commissioning/operation** if combined with statistical database from quality controls and **commissioning data**

- It also allows **better learning and understanding** of the different **systems** of a **sc magnet**, and of their **physical and technological issues** and could also enable the different **experts** to **communicate** with a **clearer** baseline

Thank you for your
attention

The logo for CEA (Commissariat à l'énergie atomique et aux énergies alternatives) features the lowercase letters 'cea' in a white, rounded, sans-serif font. A thin green horizontal line is positioned directly beneath the letters.

*/ Special thanks to A. Torre, J.L. Duchateau, L. Zani, R. Riccioli,
Q. Gorit, Q. Le Coz & I. Meziane, for fruitful discussions and support*

