



Predicting the Response of p-type Silicon Sensors to Hadron Radiation: a Hamburg Model Simulation

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Introduction

- Silicon detection is a mature technology for registering the passage of charged particles.
 - It continues to evolve toward **increasing radiation tolerance** as well as precision and adaptability.
 - Damage is known to be caused by non-ionizing energy loss.
- The high energy physics community has gradually shifted to the use of **p-type (n-in-p) silicon sensors in place of n-type (p-in-n)**.
 - p-type sensors are potentially more radiation hard and have reduced fabrication costs
- The **Hamburg Model simulation code** developed for the prediction of n-type silicon sensors in the experiments at the LHC is being adapted for **p-type silicon sensors**.
 - The alterations of the model and code base* will be discussed.

* ATLAS Collaboration, Hamburg Model Simulation Code, (2019),

<https://gitlab.cern.ch/atlas/athena/tree/master/InnerDetector/InDetCalibAlgs/PixelCalibAlgs/RadDamage/HamburgModel>

Hamburg Model: Leakage Current Simulations

- The Hamburg Model* is based on this relationship:

$$\Delta I_{\text{leak}} = \alpha \Phi_{\text{eq}} V$$

- Here, ΔI_{leak} is the difference in leakage current at fluence Φ_{eq} relative to the value before irradiation of the sensor depleted volume V , and α is the current-related damage coefficient
- And by replacing α the equation becomes**:

$$\Delta I = (\Phi_{\text{eq}}/L_{\text{int}}) \times V \cdot \sum_{i=1}^n L_{\text{int},i} \cdot \left[\alpha_I \exp\left(-\sum_{j=i}^n \frac{t_j}{\tau(T_j)}\right) + \alpha_0^* - \beta \log\left(\sum_{j=i}^n \frac{\Theta(T_j) \cdot t_j}{t_0}\right) \right]$$

- Where the variables are:

t_i is the time, and $t_0 = 1$ min

$$\alpha_I = (1.23 \pm 0.06) \times 10^{-17} \text{ A/cm}$$

$$\tau^{-1} = (1.2_{-1.0}^{+5.3}) \times 10^{13} \text{ s}^{-1} \times e^{(-1.11 \pm 0.05) \text{ eV}/k_B T}$$

$$\alpha_0^* = 7.07 \cdot 10^{-17} \text{ A/cm}$$

$$\beta = (3.29 \pm 0.18) \times 10^{-18} \text{ A/cm}$$

$$\text{and } \Theta(T) = \exp\left[-\frac{E_I^*}{k_B} \left(\frac{1}{T} - \frac{1}{T_{\text{ref}}}\right)\right]$$

* M. Moll et al., Leakage Current of Hadron Irradiated Silicon Detectors - Material Dependence. Nucl. Instrum. Meth. A, 426(87), 1999.

** ATLAS Collaboration, "Modelling radiation damage to pixel sensors in the ATLAS detector," JINST 14, P06012 (2019).

Hamburg Model: Depletion Voltage Simulations

- The Hamburg Model* proposes that the impact on **depletion voltage is dependent on irradiation and temperature** and can be determined through a **parameterized set of equations** that can be used to compute the **effective doping concentration**:

$$V_{\text{dep}} = \frac{qd^2}{2\epsilon\epsilon_0} \times |N_{\text{eff}}|$$

- The effective doping concentration can change through stable damage and initial dopant removal:

$$N_C = N_{C,0}(1 - c\Phi_{\text{eq}}) + g_C\Phi_{\text{eq}}$$

- It may also undergo short term beneficial annealing and long term annealing effects as (respectively):

$$N_A = g_A\Phi_{\text{eq}}e^{-t/\tau_a}$$

$$N_Y = g_Y\Phi_{\text{eq}}(1 - e^{t/\tau_Y})$$

- These effects are used to describe the change in effective doping concentration with respect to the initial doping concentration of the sensor

$$\Delta N_{\text{eff}} = N_C + N_A + N_Y$$

here τ_a and τ_Y ($1/k_a$ and $1/k_Y$, respectively) are defined by Arrhenius equations and have a temperature dependence. The constants g_C , g_A , g_Y are the “introduction rates” and c is the removal constant.

*M. Moll, “Radiation damage in silicon particle detectors: Microscopic defects and macroscopic properties,” Doctoral dissertation (University of Hamburg, Hamburg, Germany, 1999)

Hamburg Model as Differential Equations

- The Hamburg Model can be written as a set of differential equations that describe the change in the donor and acceptor concentrations
- This set of equations describe (initially) **n-type silicon sensors***

$$\Delta N_{\text{eff}} = N_{\text{donor}} - N_{\text{acceptor}}$$

$$= N_{\text{donor}}^{\text{non-removable}} + N_{\text{donor}}^{\text{removable}} - N_{\text{acceptor}}^{\text{stable}} - N_{\text{acceptor}}^{\text{beneficial}} - N_{\text{acceptor}}^{\text{reverse}}$$

Possible for some initial donors to be “non-removable”

Stable damage due to applied fluence

Donors

$$\frac{d}{dt} N_{\text{donor}}^{\text{removable}}(t) = -c_D \Phi_{\text{eq}}(t) N_{\text{donor}}^{\text{removable}}$$

$$\frac{d}{dt} N_{\text{acceptor}}^{\text{stable}}(t) = g_C \Phi_{\text{eq}}(t)$$

$$\frac{d}{dt} N_{\text{acceptor}}^{\text{beneficial}}(t) = g_A \Phi_{\text{eq}}(t) - k_A N_{\text{acceptor}}^{\text{beneficial}}(t)$$

$$\frac{d}{dt} N_{\text{neutral}}^{\text{reverse}}(t) = g_Y \Phi_{\text{eq}}(t) - k_Y N_{\text{neutral}}^{\text{reverse}}(t)$$

$$\frac{d}{dt} N_{\text{acceptor}}^{\text{reverse}}(t) = k_Y N_{\text{neutral}}^{\text{reverse}}(t)$$

Acceptors

Beneficial Annealing – short term ~few days

Reverse Annealing – includes an intermediate step of neutral defect sites

Temperature Dependent

*ATLAS Collaboration, “Modelling radiation damage to pixel sensors in the ATLAS detector,” JINST 14, P06012 (2019).

Hamburg Model as Implemented in Code

- The differential equations describing the time (i.e., temperature and fluence) dependence can be solved (using variation of parameters) as*:

$$\begin{aligned}\Delta N_{\text{eff}} &= N_{\text{donor}} - N_{\text{acceptor}} \\ &= N_{\text{donor}}^{\text{non-removable}} + N_{\text{donor}}^{\text{removable}} - N_{\text{acceptor}}^{\text{stable}} - N_{\text{acceptor}}^{\text{beneficial}} - N_{\text{acceptor}}^{\text{reverse}}\end{aligned}$$

$$N_{\text{donor}}^{\text{removable}} = N_{\text{donor},0}^{\text{removable}} (1 - e^{-\Phi_{\text{eq}}^{\text{rate}} t})$$

$$N_{\text{acceptor}}^{\text{stable}} = g_C \Phi_{\text{eq}}^{\text{rate}} t$$

$$N_{\text{acceptor}}^{\text{beneficial}} = \frac{g_A}{k_A} \Phi_{\text{eq}}^{\text{rate}} (1 - e^{-k_A t}) + N_{\text{acceptor},0}^{\text{beneficial}} e^{-k_A t}$$

$$N_{\text{neutral}}^{\text{reverse}} = \frac{g_Y}{k_Y} \Phi_{\text{eq}}^{\text{rate}} (1 - e^{-k_Y t}) + N_{\text{neutral},0}^{\text{reverse}} e^{-k_Y t}$$

$$N_{\text{acceptor}}^{\text{reverse}} = \frac{g_Y}{k_Y} \Phi_{\text{eq}}^{\text{rate}} (k_Y t + e^{-k_Y t} - 1) + N_{\text{neutral},0}^{\text{reverse}} (1 - e^{-k_Y t})$$

- The model is run over discrete timesteps
- The input at each timestep:
 - Duration of the timestep (t)
 - Fluence rate in the timestep (Φ_{eq})
 - Temperature during the timestep (T)
- The subscript “0” refers to the concentration (N) at the beginning of the timestep

Arrhenius equation

(introduction of temperature dependence)

$$k_i = k_{i,0} e^{-E_i/k_B T}$$

$$E_A = 1.09 \pm 0.03 \text{ eV}, E_Y = 1.33 \pm 0.03 \text{ eV}$$

$$k_{A,0} = 2.4_{-0.8}^{+1.2} \times 10^{13} / \text{s} \text{ and } k_{Y,0} = 1.5_{-1.1}^{+3.4} \times 10^{15} / \text{s}$$

Donor Removal Constant†

$$c = 10.9 \text{ cm}^{-2} / N_{\text{eff},0}$$

Introduction Rates

Fit to ATLAS B-Layer Data**

$$g_C = 0.6 \times 10^{-2} / \text{cm}$$

$$g_A = 6.0 \times 10^{-2} / \text{cm}$$

$$g_Y = 0.43 \times 10^{-2} / \text{cm}$$

* J.C. Beyer, Doctoral dissertation, MPI Munich (Mar. 2019).

† M. Moll, Doctoral dissertation (University of Hamburg, Hamburg, Germany, 1999)

** <https://atlas.web.cern.ch/Atlas/GROUPS/PHYSICS/PLOTS/PIX-2018-005/>

Hamburg Model for p-type Sensors

“The acceptor removal process [...] has become the field of high interest due to the recent shift from n-type to p-type silicon devices in the HEP community”*

- Complete characterization of p-type is still ongoing in our community.
- Some changes to the n-type model are necessary:
- Introduce an initial acceptor removal term and remove the initial donor term:

$$N_{\text{donor}}^{\text{removable}} = N_{\text{donor},0}^{\text{removable}} (1 - e^{-c\Phi_{\text{eq}}^{\text{rate}}t}) \quad \longrightarrow \quad N_{\text{acceptor}}^{\text{removable}} = N_{\text{acceptor},0}^{\text{removable}} (1 - e^{-c^{\text{acceptor}}\Phi_{\text{eq}}^{\text{rate}}t})$$

- Annealing terms have generally been neglected in previous studies

$$N_{\text{acceptor}}^{\text{beneficial}} = \frac{g_A}{k_A} \Phi_{\text{eq}}^{\text{rate}} (1 - e^{-k_A t}) + N_{\text{acceptor},0}^{\text{beneficial}} e^{-k_A t}$$

$$N_{\text{neutral}}^{\text{reverse}} = \frac{g_Y}{k_Y} \Phi_{\text{eq}}^{\text{rate}} (1 - e^{-k_Y t}) + N_{\text{neutral},0}^{\text{reverse}} e^{-k_Y t}$$

$$N_{\text{acceptor}}^{\text{reverse}} = \frac{g_Y}{k_Y} \Phi_{\text{eq}}^{\text{rate}} (k_Y t + e^{-k_Y t} - 1) + N_{\text{neutral},0}^{\text{reverse}} (1 - e^{-k_Y t})$$

* M. Moll, IEEE Trans. Nucl. Sci. 65, 1561–1582 (2018).

** G. Kramberger et al., Initial acceptor removal in p-type silicon, TRENTO Workshop, 2015.

*** R. Wunstorff et. al, Nucl. Instr. and Meth. A 377, 228– 233 (1996).

Terms for the p-type Model

- The effective doping concentration as a function of fluence for p-type sensors can be expressed as^{†,‡}:

$$N_{\text{eff}} = N_{\text{eff},0} - N_{\text{C}}(1 - \exp(-c_{\text{A}}\Phi_{\text{eq}})) + g_{\text{C}}\Phi_{\text{eq}}.$$

[†]B. Hiti et al., Nucl. Instruments Methods Phys. Res. Sect. A 924, 214–218 (2019).

[‡]G. Kramberger et al., Initial acceptor removal in p-type silicon, TRENTO Workshop, 2015.

Terms for the p-type Model

- The effective doping concentration as a function of fluence for p-type sensors can be expressed as^{†,‡}:

$$N_{\text{eff}} = N_{\text{eff},0} - N_C(1 - \exp(-c_A \Phi_{\text{eq}})) + g_C \Phi_{\text{eq}}$$

Initial doping concentration
typical values are:

$$N_{\text{eff},0} = 2 \times 10^{12} \text{ cm}^{-3}$$

for 3D p-type sensor

Stable initial acceptor
removal term, expressed in
the simulation code as:

$$N_{\text{acceptor}}^{\text{removable}} = N_{\text{acceptor},0}^{\text{removable}} (1 - e^{-c_A \Phi_{\text{eq}}^{\text{rate}} t})$$

Stable effective acceptor
introduction term, expressed
in the simulation code as:

$$N_{\text{acceptor}}^{\text{stable}} = g_C \Phi_{\text{eq}}^{\text{rate}} t$$

- Note that the annealing terms are excluded in this expression

*M. Moll, IEEE Transactions on Nuclear Science, 65 8 (2018).

†B. Hiti et al., Nucl. Instruments Methods Phys. Res. Sect. A 924, 214–218 (2019).

‡G. Kramberger et al., Initial acceptor removal in p-type silicon, TRENTO Workshop, 2015.

p-type Model Parameters

- There are three parameters to set in p-type model

$$N_{\text{eff},0} = 2 \times 10^{12} \text{ cm}^{-3}$$

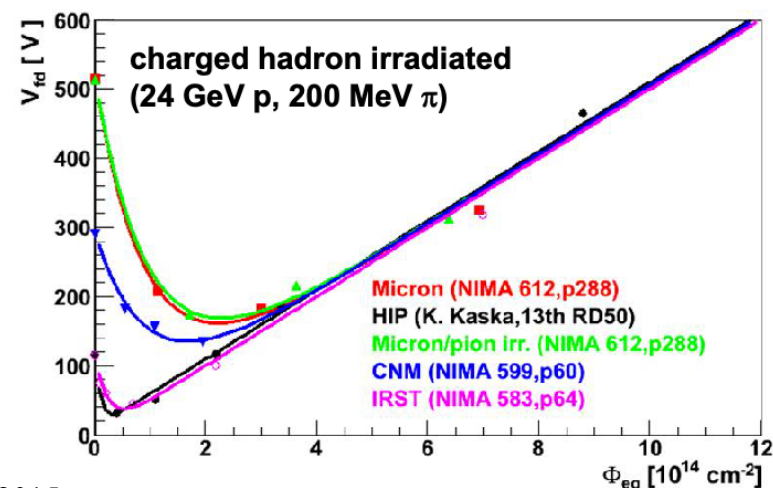
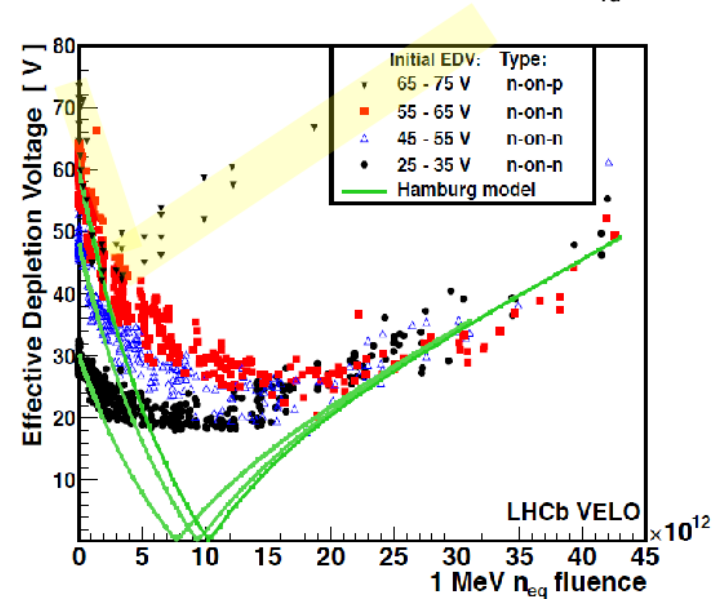
$$N_{\text{eff}} = N_{\text{eff},0} - N_{\text{C}}(1 - \exp(-c_{\text{A}}\Phi_{\text{eq}})) + g_{\text{C}}\Phi_{\text{eq}}$$

1. Number of initial acceptors that can be removed
2. Acceptor removal constant
3. Acceptor introduction rate

Parameter Values (1)

1. N_C - acceptors that can be removed
 - Naively, we expect complete initial acceptor removal: $N_{C0}/N_{\text{eff},0} = 1$
 - Incomplete acceptor removal has been observed in some devices, with values as low as: $N_{C0} = 0.1 \times N_{\text{eff},0}$
 - Studies have suggested that the value of N_C may be dependent on radiation type
 - The figures[‡] on the right show (upper) the LHCb and (lower) individual experiments' depletion voltage measurements
 - In the p-type sensors shown in the figures one can see the initial decrease in acceptors followed by an increase
 - At some point the acceptor removal term of the model becomes negligible

- LHCb Velo uses n-p sensor and has observed the effect of removal in V_{fd}



[‡]G. Kramberger et al., Initial acceptor removal in p-type silicon, TRENTO Workshop, 2015.

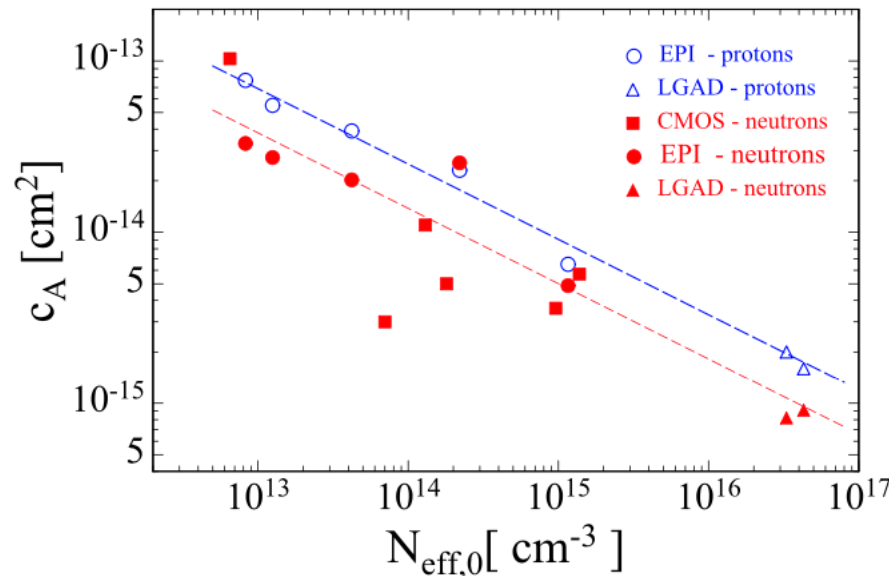
Parameter Values (2)

2. c_A – acceptor removal constant

- The value of c_A has been determined to be*:

$$c_A = 1.98 \times 10^{13} \text{ cm}^2$$

- This is consistent with the results presented in the figure† and an initial doping concentration of $N_{\text{eff},0} = 2 \times 10^{12} \text{ cm}^{-3}$



*R. Wunstorf, W. M. Bugg, J. Walter, F. W. Garber, and D. Larson, “Investigations of donor and acceptor removal and long term annealing in silicon with different boron/phosphorus ratios,” Nucl. Instr. and Meth. A 377, 228– 233 (1996)

†M. Moll, IEEE Transactions on Nuclear Science, 65 8 (2018).

Parameter Values (3)

3. g_C – acceptor introduction rate^{*,†}: 0.02 cm^{-1}
 - Other values as low as 0.01 cm^{-1} are presented in [^{*}]
 - The value fit with ATLAS data[‡] for n-type sensors (on the B-Layer) is 0.0043 cm^{-1}

* V. Cindro et al., “Radiation damage in p-type silicon irradiated with neutrons and protons,” NIMA 599, 60–65 (2009).

† G. Lindström et al., “Radiation hard silicon detectors - developments by the RD48 (ROSE) Collaboration,” Nucl. Instr. and Meth. A 466, 308 (2001).

‡ <https://atlas.web.cern.ch/Atlas/GROUPS/PHYSICS/PLOTS/PIX-2018-005/>

Introducing Annealing

- Ignore short term beneficial annealing*:
 - “the resulting annealing rate was less than 1% of the acceptor removal rate, in most cases zero, which indicates that there is no significant short term room temperature annealing”
- Introduce long term reverse annealing analogous to the n-type simulation, with these two terms:

$$N_{\text{neutral}}^{\text{reverse}} = \frac{g_Y}{k_Y} \Phi_{\text{eq}}^{\text{rate}} (1 - e^{-k_Y t}) + N_{\text{neutral},0}^{\text{reverse}} e^{-k_Y t}$$

$$N_{\text{acceptor}}^{\text{reverse}} = \frac{g_Y}{k_Y} \Phi_{\text{eq}}^{\text{rate}} (k_Y t + e^{-k_Y t} - 1) + N_{\text{neutral},0}^{\text{reverse}} (1 - e^{-k_Y t})$$

- g_Y is taken from the ATLAS n-type simulation: $g_Y = 6.0 \times 10^{-2} / \text{cm}$.

*R. Wunstorf, W. M. Bugg, J. Walter, F. W. Garber, and D. Larson, “Investigations of donor and acceptor removal and long term annealing in silicon with different boron/phosphorus ratios,” Nucl. Instr. and Meth. A 377, 228– 233 (1996)

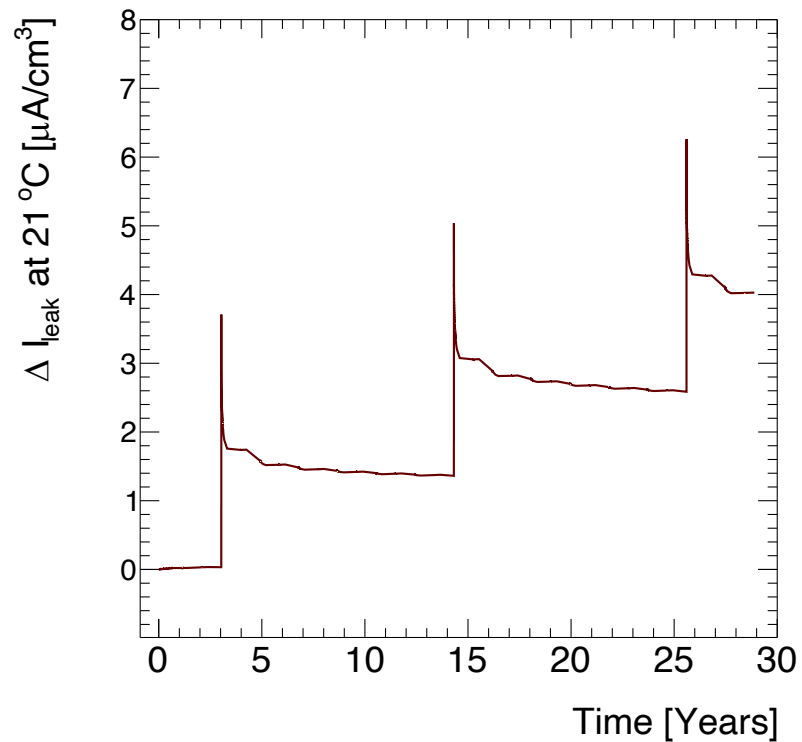
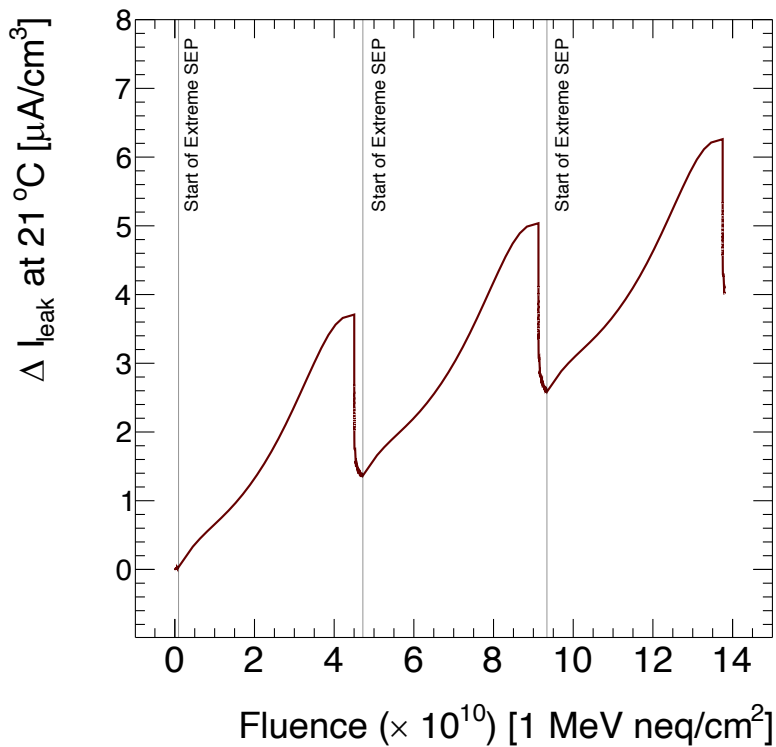
† M. Moll, IEEE Transactions on Nuclear Science, 65 8 (2018).

Conditions for the Simulation

- The model is run over discrete timesteps and the input at each timestep is:
 1. Duration of the timestep (t)
 2. Fluence rate in the timestep (Φ_{eq})
 3. Temperature during the timestep (T)
- The investigations presented here are for:
 - Each time step set to 1 min, for a total integrated time of tens of years
 - Continuous, low fluence rate ($5.2 \text{ neq/cm}^2/\text{sec}$) and three higher fluence rates ($4.98 \times 10^5 \text{ neq/cm}^2/\text{sec}$) applied at equally separated time intervals
 - Total integrated fluence applied is about $1.4 \times 10^{10} \text{ neq/cm}^2$
 - A yearly and daily temperature cycle with a mean below $0 \text{ }^\circ\text{C}$ and a maximum of $25 \text{ }^\circ\text{C}$
- Compare simulation results for n-type and p-type sensors where the electrode spacings are set as:
 - 250 microns for n-type sensors
 - 40 microns for p-type sensors (representing an approximation to 3D sensors)

Leakage Current Results

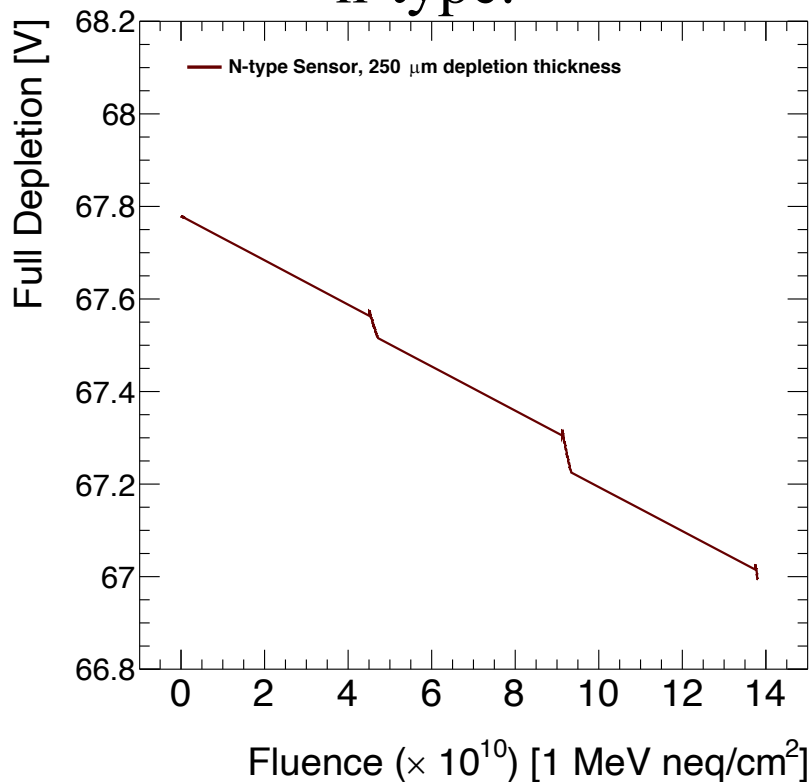
- The leakage current results of the simulation are shown here.
 - The higher fluence rate events dominate the picture
- Results are the same for both n-type and p-type sensors



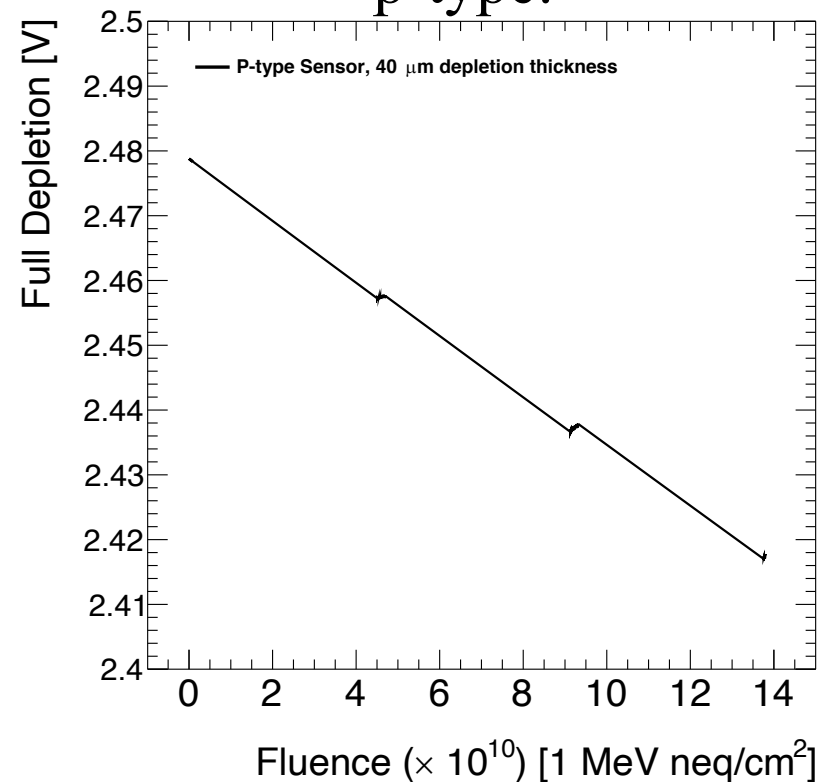
n-type and p-type Depletion Voltage Simulations

- The simulation results for (left) the n-type sensor and (right) the p-type sensor are shown here
 - The discontinuities reflect the effects of reverse annealing after cessation of the higher fluence events

n-type:

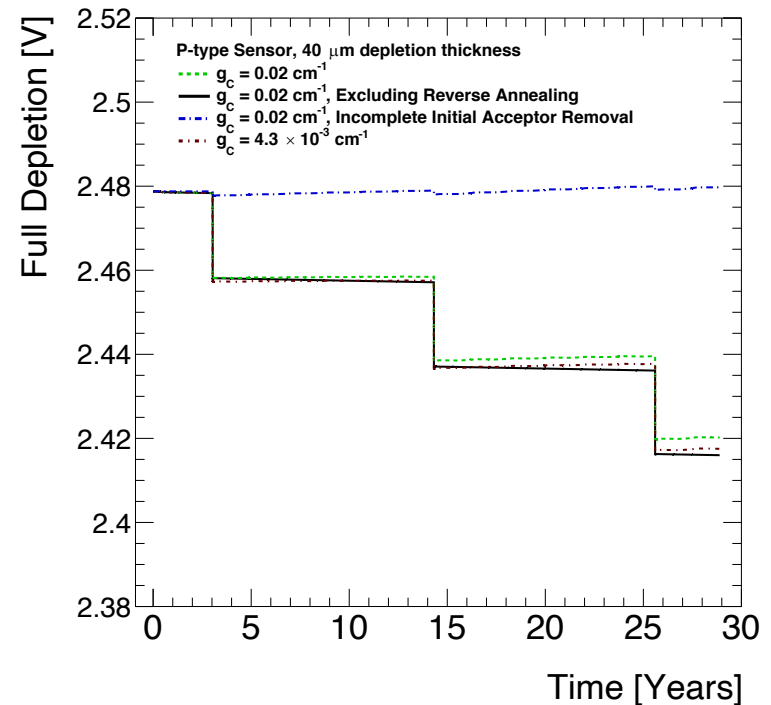
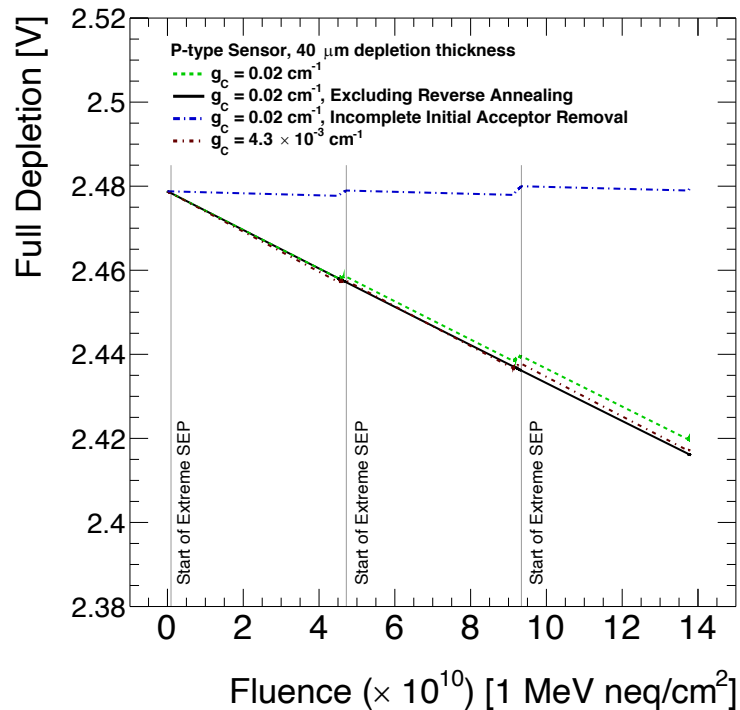


p-type:



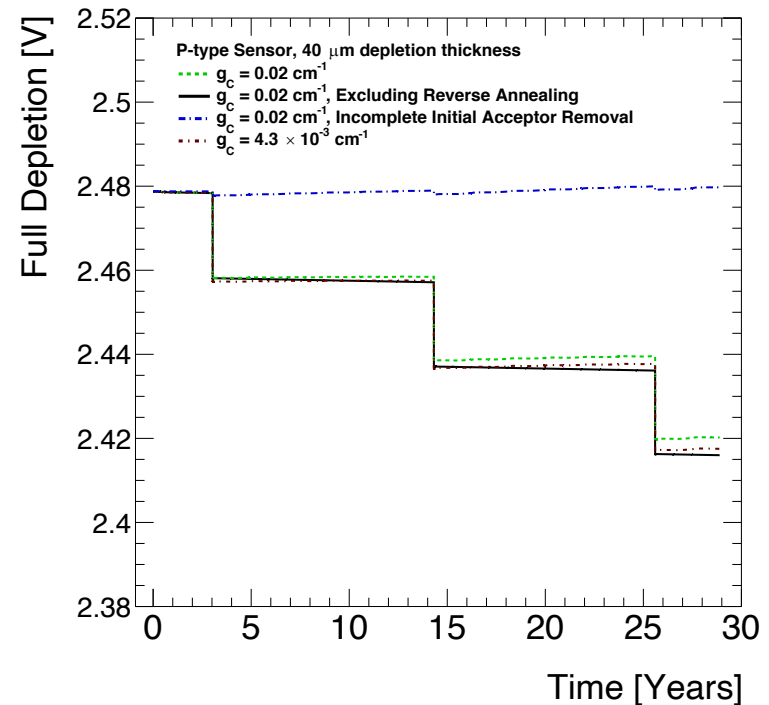
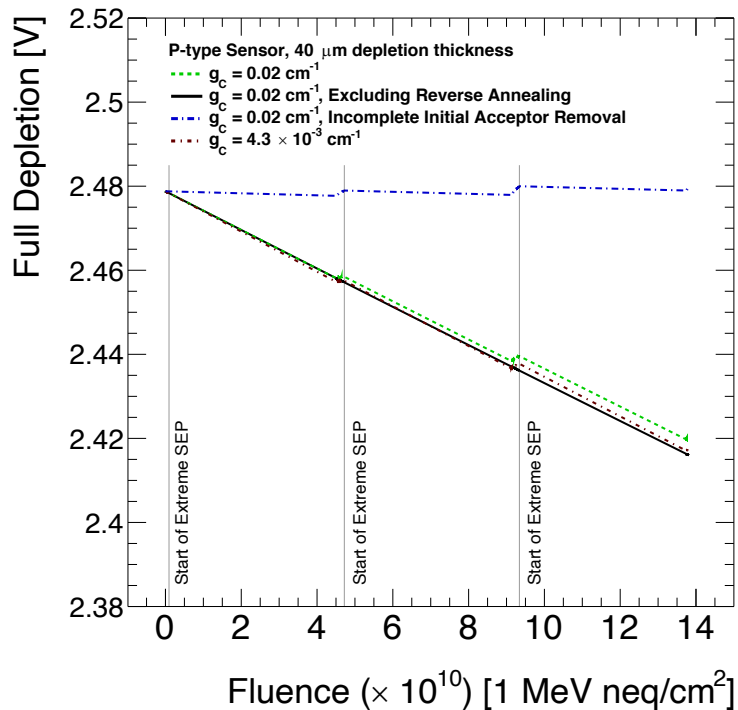
p-type Depletion Voltage Simulations

- Want to probe the simulation by using different parameter values: the p-type simulations for four different parameter settings are shown here
 - Nominally, $g_C = 0.02 \text{ cm}^{-1}$ and potential for complete acceptor removal is assumed
- (Left plot) simulation of depletion voltage for p-type sensors versus fluence
- (Right plot) simulation of depletion voltage for p-type sensors versus time



p-type Depletion Voltage Simulations - Results

- Reverse annealing plays a role for these time scales – this can be seen by comparing the black line (which excludes the reverse annealing terms) to the green dotted line
- The impact of changing g_C for the bounds of the range of values used in previous experiments is investigated – this can be seen by comparing the red dotted line ($g_C = 4.3 \times 10^{-3} \text{ cm}^{-1}$) to the green dotted line ($g_C = 0.02 \text{ cm}^{-1}$)
- Once the initial acceptor removal is exhausted, the effective acceptor introduction term will dominate subsequent behavior, and the slope will become positive – this is observed in the incomplete acceptor removal scenario in the blue dotted line



Conclusions and Outlook

- An overview of the **response of p-type silicon sensors** to non-ionizing energy loss and a new simulation of these effects has been discussed.
- Initial results for p-type simulations have been presented including **reverse annealing in the simulation**, **accounting for incomplete initial acceptor removal**, and **varying the acceptor introduction rate** for the bounds of the range of values used in previous experiments.
- Further studies of the impact due to different radiation and temperature environments will be investigated and compared to test beam data.
 - Other parameters in the model can be constrained when compared to physical data.
- Will be able to use this simulation code to describe characteristic data of irradiated silicon sensors and project the effects of further irradiation **in future experiments**