Charge collection efficiency of a thinned, backside biased, neutron irradiated High Voltage-CMOS active matrix

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Motivation

The proposed 10x luminosity upgrade of the Large Hadron Collider (LHC) is just one example of the field moving forward with respect to particle energies and rates.

High Voltage CMOS is designed to be radiation tolerant, highly granular with small monolithic active pixels and able to be thinned for minimum interaction with experimental particles trajectories.

One must characterize what has been achieved with the technology so far to determine how to further develop it.



HVPixel1: 2006



H35DEMO: 2016

H35DEMO

- 4 Matrices Active monolithic pixels (No external readout ASIC)
- Designed in the 0.35 µm process from AMS
- 100 μm thin
- Chip dimensions are 24.40 mm x 18.49 mm
- Backside biased
- Substrate resistivities (20 $\Omega \cdot cm$, 80 $\Omega \cdot cm$, 200 $\Omega \cdot cm$, **1000 \Omega \cdot cm**)
- 300 columns and either 16 or 23 rows of pixels per matrix
- Pixel size 250 x 50 μm







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H35DEMO

- From TCAD simulations, we know that with thinned, backside biased sensors produced in high resistivity substrate have:
 - Stronger electric field lines
 - Shorter charge collection times
 - Potentially better radiation tolerance







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- 2. Use radioactive sources to stimulate the sensing junction 1.6 μ s with 1024 sampling points using a DRS4 board to digitize analogue signal
- 3. Trigger on analogue output itself -> Find a way to determine real vs dark hits

Charge Injection

Firstly the CSA electronics have been tested using a 0 - 5 V square wave test pulse through the injection circuit.

The injection circuit does not use the sensing junction of the sensor.

Therefore the charge collected should not depend on the bias voltage used, but a standard shaped signal output is expected.



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Sr90 Testing

Source measurements are expected to give a spectrum of response which is seen but we see a much larger spreads at low energies.

Source is collimated to a thin beam but still emits in an area larger than a single pixel, some responses are seen from pixels neighbouring the readout pixels.



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Monitor Line Setup

The analogue matrices have 3 monitor outputs and 1 amplifier output (AnalogOut) meaning the 3 adjacent pixels can be read out simultaneously.

AnalogOut \rightarrow Output of the pixel after the source follower (SFOut) + one buffer at the periphery.

Monitor \rightarrow Output of the pixel after the output buffer (Test) + one buffer at the periphery







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Conversion Ratio



The X-rays produced by the Fe-55 source create electron/hole pairs in the depletion region.

 $\frac{X - ray (5.9 \ keV)}{e - h \ production (3.6 \ eV)} = 1639 \ electrons$

Full Depletion has an average output voltage of 25.51 mV for each hit creating 1639 electrons.

 $Conversion = 64.25 \underline{e}_{\overline{mV}}$

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High Voltage Range to Measure



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Charge Collection Efficiency dependence on fluence



Charge Collection Efficiency dependence on fluence



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Summary and Goals

At Liverpool we have established and tested apparatus for measuring the charge collection efficiencies of irradiated sensors.

We have investigated the charge collection efficiencies of the a high resistivity, thinned and backside biased HV-CMOS sensor to fluences comparable to that inside large high energy physics experiments.

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This experiment is ongoing and we have fluences up of 1 \times 10^{16} \frac{n_{eq}}{cm^2} and 2 \times 10^{16} \frac{n_{eq}}{cm^2} still to test
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Thank you all for listening!

Any Questions?

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DAC settings



DAC	Use Value		
6	BLR	15	
7	VPAB	5	
8	VNFB	40	
12	VNLogic	1	
13	VPLoad	24	
14	VNSF	15	
15	VP	50	
16	VPAB	60	

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PMT removal

It was chosen to trigger on the analogue output after the following was observed:

- The PMT would trigger when a particle went through an unwanted pixel creating more useless data.
- Good hits were often made unusable by a time delay which caused a section of the waveform to be lost outside of the trigger window





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Finding output voltage – charge collected conversion factor

The injection circuit does not use the sensing junction of the sensor and therefore the charge collected should not depend on the bias voltage used.

For Sr90 however:

This is what we should expect:

- Sensor reaches a bias voltage where it is fully depleted.
- From eTCT measurements we know the depletion width at these bias voltages



Finding output voltage – charge collected conversion factor



This is a plot from a cadence simulation in which the simulation gives the voltage measured by the scope as a function of the charge collected by the sensor.

This gain will be used to convert all voltage outputs into charge collected.

Where:
$Q_{detector} = Charge in pixel$
$C_{detector} = Capacitance of pixel = 442 fF$
$V_{nw} = voltage \ change \ in \ nwell$
$G_{CSA} = gain \ of \ amplifier = 38.619 \frac{\mu V}{e^{-1}}$
$e_{detector} = amount of electrons collected$

Fe55 X-ray Attenuation



M.Franks:

E-TCT characterization of a thinned, backside biased, irradiated HV-CMOS pixel test structure

X-ray energy from Fe55 will give a constant energy response.

Linear attenuation
$$E = E_0 e^{-\mu x}$$

$$\mu = \sim 147 \frac{cm^2}{g} \times 2.329 \frac{d}{cm^3} = 340 \ cm^{-1}$$

$$\frac{E}{E_0} = e^{-340 \times 0.01 \, cm} = 0.3 = \sim 3\% \text{ energy remaining}$$

97% of energy is deposited into sensor when fully depleted



