

Testing Electronics for Fusion Application



focus on neutrons

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The main scope of this presentation is the test of SEEs induced by neutrons on electronics intended to be operated in a neutron flux near a fusion reactor (DD or DT plasma neutrons).

Regardless of the intensity of the gamma and neutron fluxes, this presentation focuses on the energy spectra of neutrons and its effects, whose energy degradation can vary from one place to another in the reactor building depending on the elastic and inelastic interactions of neutrons with the surrounding structures, such as shields and walls.

Although the neutron fluxes depend on the design of the machine and the building as well as the operation of the reactor, the energy spectra of the neutrons should be quite similar in fusion reactors. Analogies but also differences can be evoked comparing with the case of Fission reactors and with the well described case of the natural atmospheric neutron spectrum.

Outline

- **About Fusion and about Tokamaks. Main types and sizes.**
- **Fusion degraded spectra behind shields**
- **Effects on Electronics**
 - Focus on neutron SEE testing according to degraded spectra behind shields
- **Testing plan in conformity with the required spectrum**
 - Which neutron test beams for which application required degraded spectrum?

Some References Concerning designs and radiations in Fusion Technology

USEFUL JOURNALS, PAPERS and books

Fusion Engineering and Research, Review of Scientific Instruments, IEEE Trans on Nuclear Science, IEEE Trans on Plasma Science

- Cited in this talk in chronology order:
 - „**Diagnostic components in harsh radiation environments: Possible overlap in R&D requirements of inertial confinement and magnetic fusion systems**“, J.-L. Bourgade, Alan Costley, Roger Reichle, J.L. Leray, M. Dentan and coll., Review of Scientific Instruments 79(10):10F304-10F304-5 (2008) DOI: 10.1063/1.2972024
 - „**Generic diagnostic issues for a burning plasma experiment**“, G. Vayakis, E. R. Hodgson, V. Voitsenya, C. I. Walker, Fusion Science and Technology vol. 53 Chapter 12, Feb. 2008, pp 699-750
 - „**Towards Diagnostics for a Fusion Reactor**“, Alan E. Costley, IEEE Transactions on Plasma Science, Vol. 38, no. 10, October 2010, 2934.
 - „**Soft Errors, from particles to circuits**“, Jean-Luc Autran and Daniela Munteanu, CRC Press, 2015
- Most recent PhD Thesis: Matteo Cecchetto, **Experimental and simulation study of neutron - induced Single Event Effects in accelerator environment and implications on qualification approach**, CERN & ISE-Montpellier Univ., April 2021
- **THE ITER PUBLIC WEBSITE** <https://www.iter.org/>

The ITER Organization provides images and videos on its public website free of charge for educational and institutional use <https://www.iter.org/album/>

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Early times of fusion

The science and physics of nuclear fusion started in the 1920s

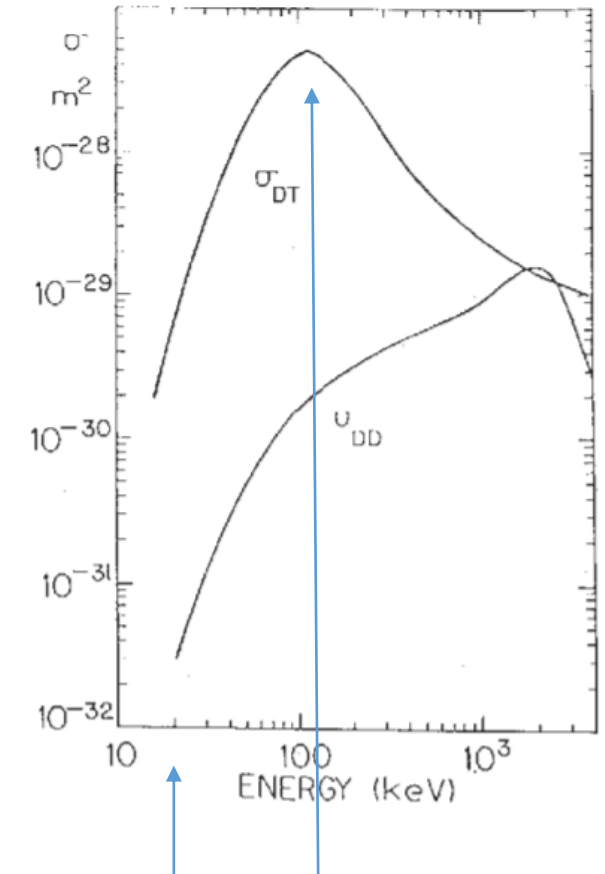
- 1926 British astrophysicist Arthur Eddington suggested that stars draw their energy from the fusion of hydrogen into helium ⁽¹⁾ => modern theoretical astrophysics (Bethe cycle of fusion in Stars)
- 1934 Rutherford showed the fusion of deuterium, and observed that "an enormous effect was produced" during the process.
- His student Mark Oliphant used an updated version of the equipment firing deuterium rather than hydrogen and discovered helium-3 by $D(d, n)^3\text{He}$ and tritium by $D(d, p)^3\text{H}$, showing that heavy hydrogen nuclei could be made to react with each other.

This was the first direct demonstration of fusion in the lab.

Just later Deuteron accelerators in the range of 100 keV were developed and ARE commonly used BY us to produce n by DD and DT reaction (many instances in our Labs)

DD and later DT plasma (atmospheric pressure) may reach the onset of fusion with large production of energy.

Threshold are ~20 keV (200 megaKelvins),
cross section max at ~100 keV (DT), 2 MeV (DD).



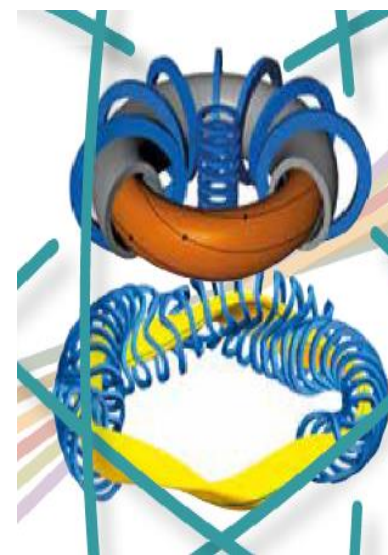
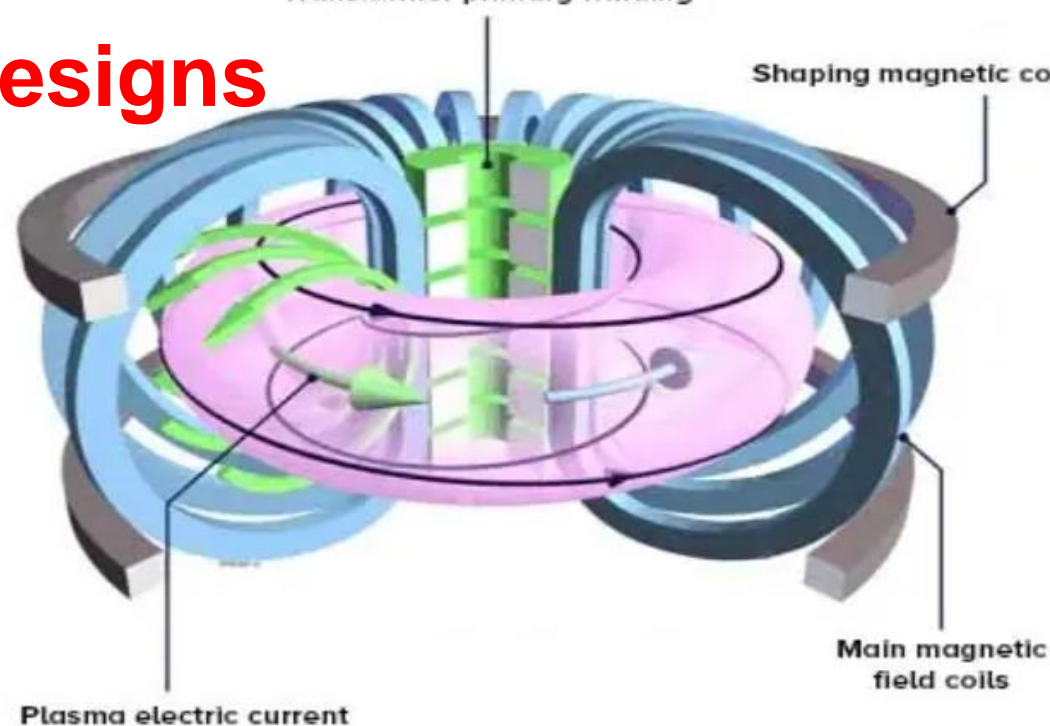
⁽¹⁾ A. Eddington, Internal Constitution of the Stars, 1926

As soon as in the 1950s, Machine designs

By the 1950s, looking at possibilities of replicating the process of nuclear fusion on Earth.

In 1950 soviet scientists **Andrei Sakharov** and **Igor Tamm** proposed the design for a type of magnetic confinement fusion
=> **TOROIDAL** device, the tokamak.

1968: hydrogen plasma at 10 million degrees, never reached before.



Helicoidal vs toroidal?
Soviet scientist Lev Artsimovich showed that the tokamak was a more efficient concept

Russian acronym

Toroidalnaya Kamera s Magnitnymi Katushkami

<https://ccfe.ukaea.uk/fusion-energy/how-fusion-works/>

TOKAMAK with neutron yield (DT) since the 80's

$Q = \text{Fusion} / \text{Heating}$ ("the gain")

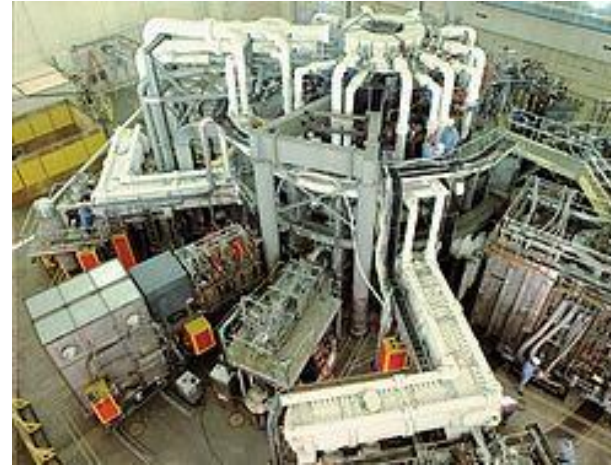
1986: Tokamak Fusion Test Reactor, Princeton, USA, produced the first 'supershots' which produced many fusion neutrons (0,2) – decommissioned 2002

1994, Princeton's Tokamak Fusion Test Reactor (TFTR) produced a world-record **10,7 MW of fusion**

1997: JET, UK near Oxford, several Deuterium-Tritium shots with Fusion ($Q=0,7$ 16 MW of Fusion power)

Under construction since 2006 – Iter undertaking in construction, worldwide cooperation
- To be renewed in 2021?

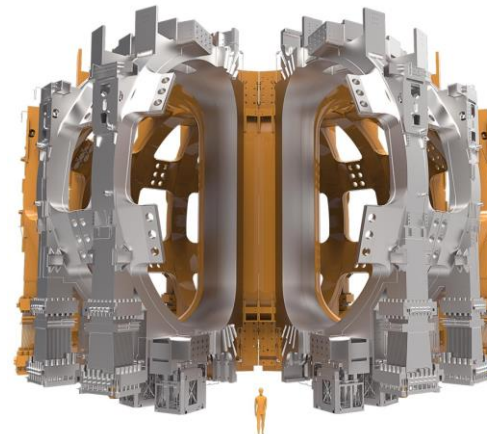
International Thermonuclear Experimental Reactor 2035 and beyond to 500 MW



TFTR, in Princeton



JET, UK in Culham near Oxford

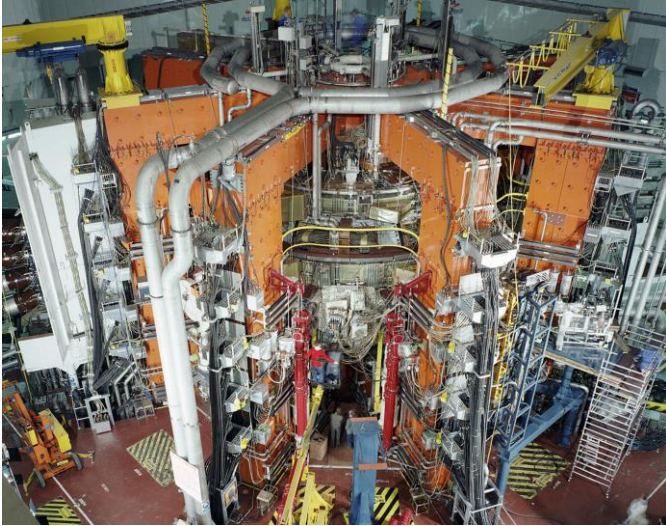


Iter in Aix-En-Provence near Marseilles, France

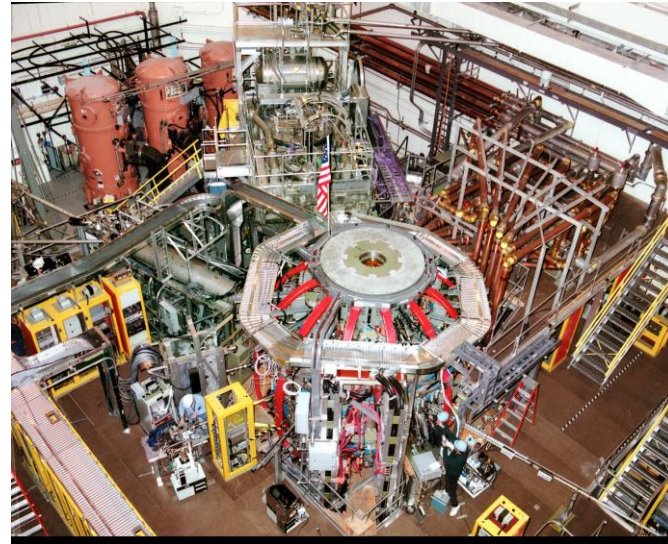
The Way to Fusion

More than 200 TOKAMAKS around the World

Several structures of tokamaks and and related designs



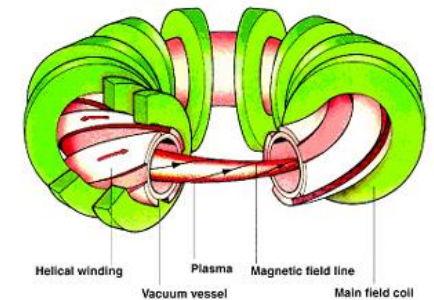
The JET toroid (1991)
Culham, UK
Classical coils



The NSTX Spherical
Princeton, USA since 2002
Classical coils



Wendelstein 7-X helix stellarator
Planck Institut (2011)



15 m diameter
440 t
30 superconducting coils

Fusion for Energy..

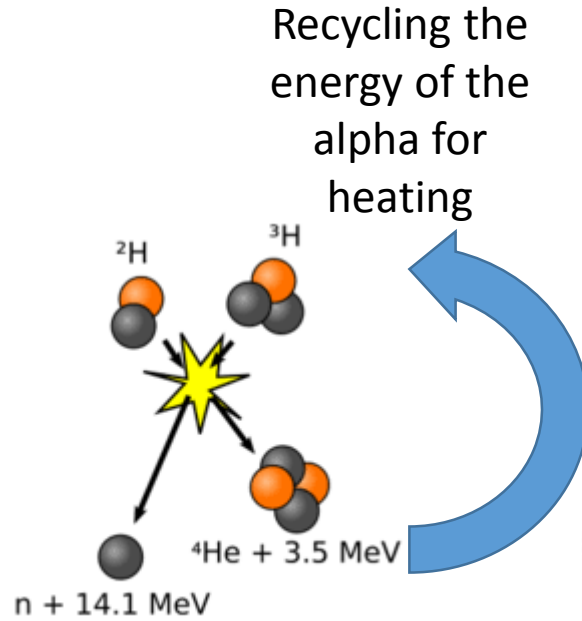
- The DEMO concept (DEMONstrator)
500 MW continuous

Envisaged circa 2100

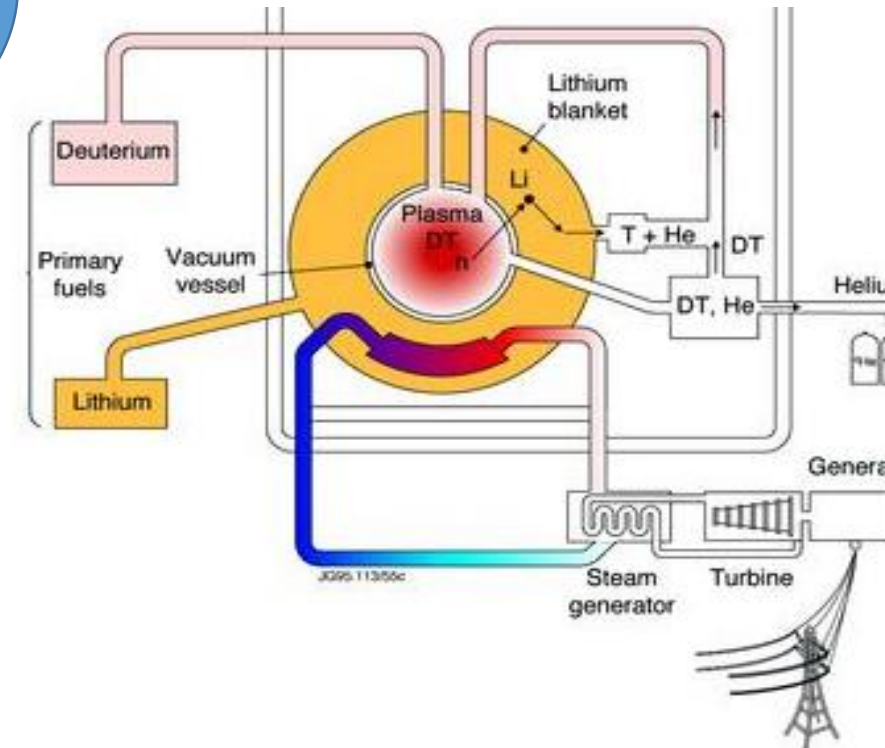
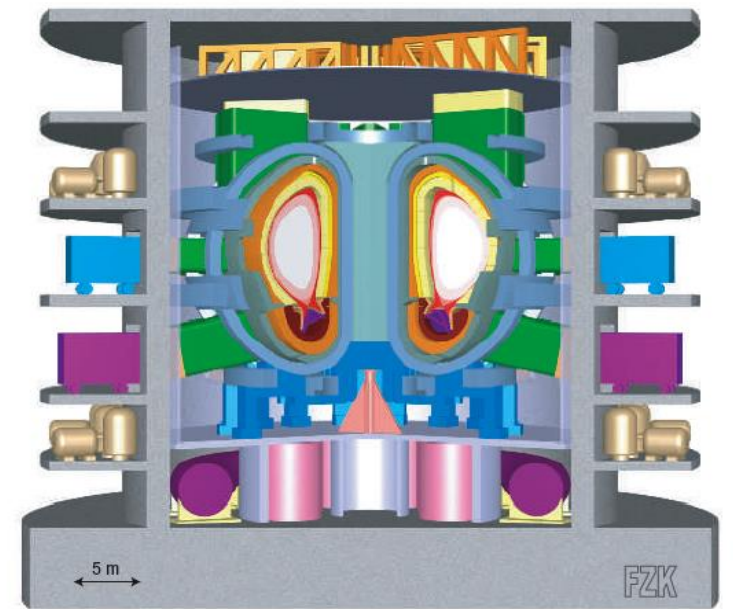
Needs self sustained balance of energy
(production = loss + extraction)

Plasma mixture, temperature
Density, volumes, losses

Many steps before



OUTPUT of the neutron energy
THROUGH
THE WALLS TO THE EXCHANGER



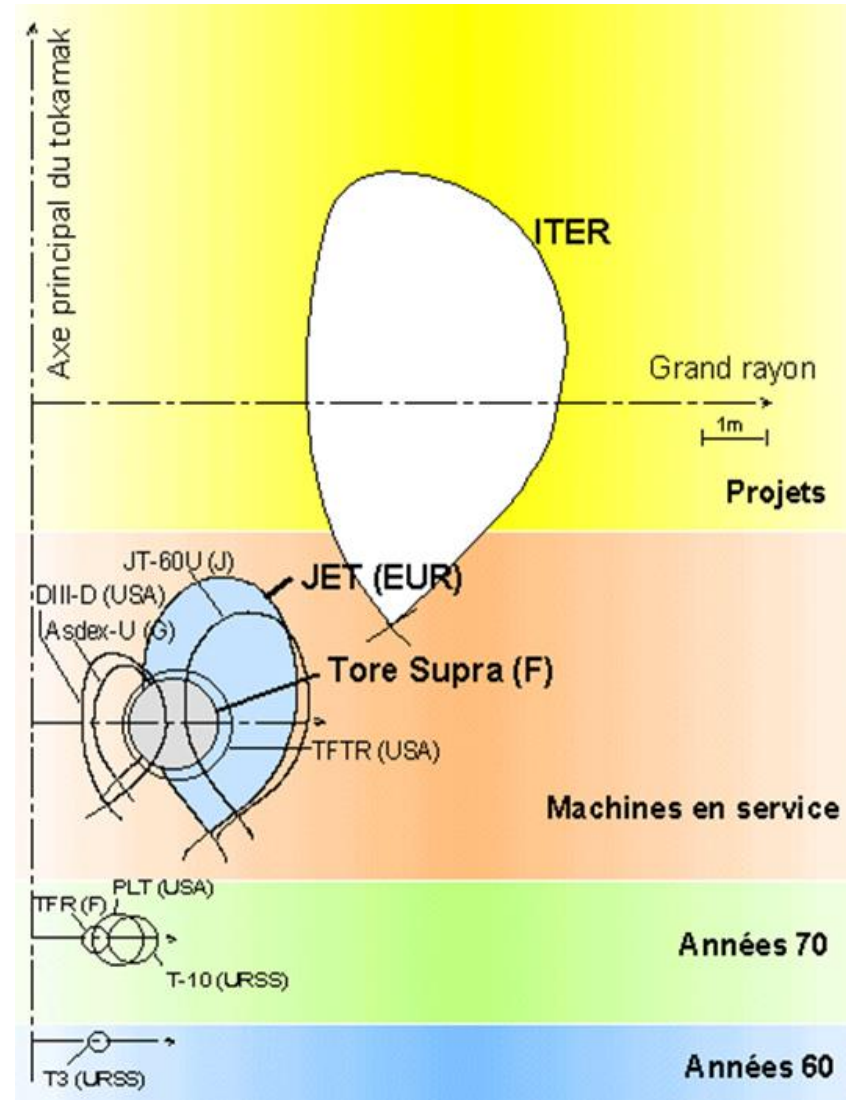
LARGE MACHINES

To improve the GAIN (Q) the balance LOSS/INPUT and increase the stability

- **JET, UK**

Joint European Tokamak
(Culham near Oxford)

- $Q=0,67$: 6 MW fusion/24 MW injected, some 10s seconds



- **Iter**

Cadarache near Aix-En-Provence

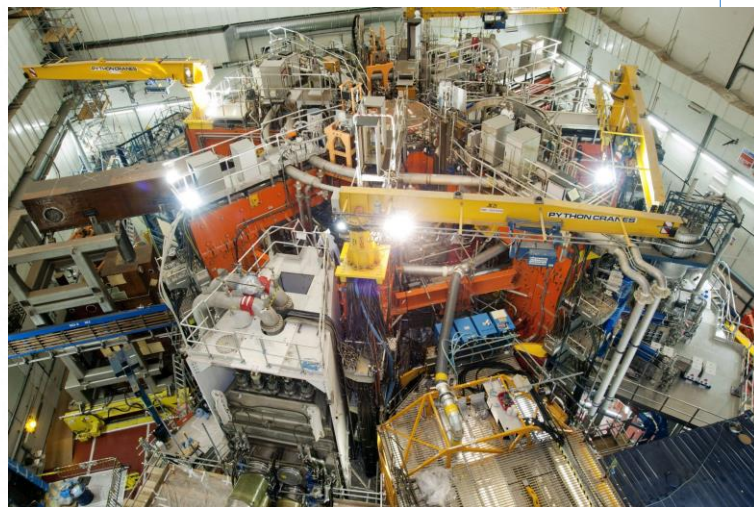
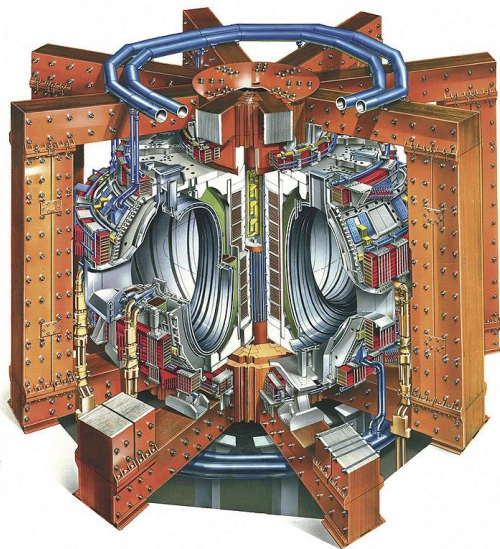
- Characteristics:
 - $Q=10$: 500 MW fusion power with only 50 MW external heating
 - Single discharge duration: 500s;
 - ~30 years exploitation
- Phases
 - 2025 H2
 - 2035 DT
- Expected accumulated total active plasma burn 0.6 years
 - 20 000 Discharges (shot)
 - accumulated total burn 0.6 years = 4700 h

- TID, DDD, SEE

UK fast track: at Culham Centre for Fusion Energy

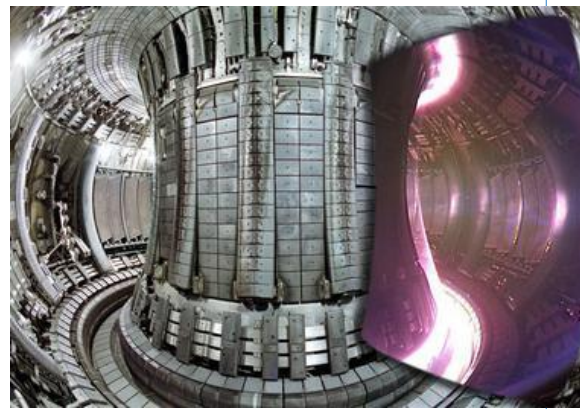
(Oxfordshire)

the JET since 1983 and the STEP (step forward To 2040)



The UK is also starting the design of a more compact, spherical fusion power plant – the Spherical Tokamak for Energy Production (STEP).

STEP builds on experience of operating and we are just embarking on a five year initial design phase, in collaboration with UK industry and academia. STEP aims to be generating electricity (>100MW) on a timescale of 2040.



LARGE MACHINES

USE OF SUPERCONDUCTING COILS

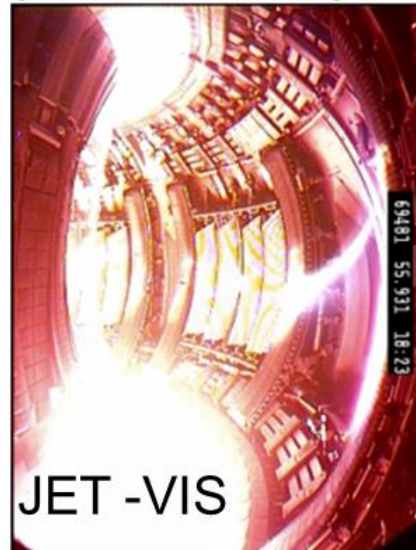
Joint Experimental Thermonuclear
Near Oxford, UK

1 second Deuterium-Tritium fusion
Achieved mid-90's

You can watch the plasma glow
(**DT burning plasma**)

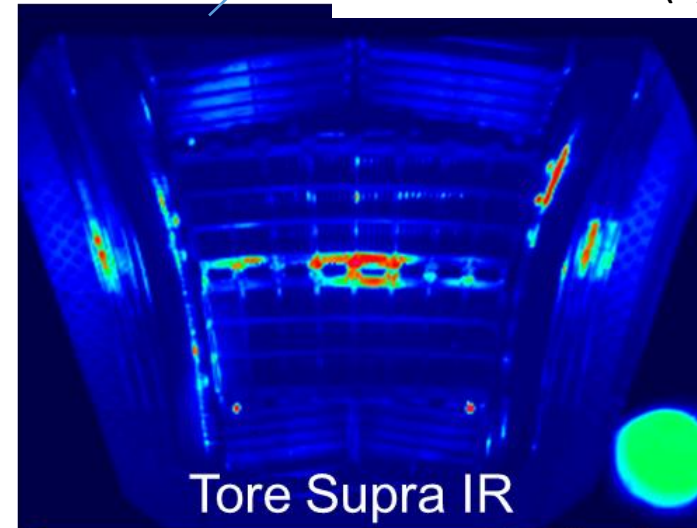
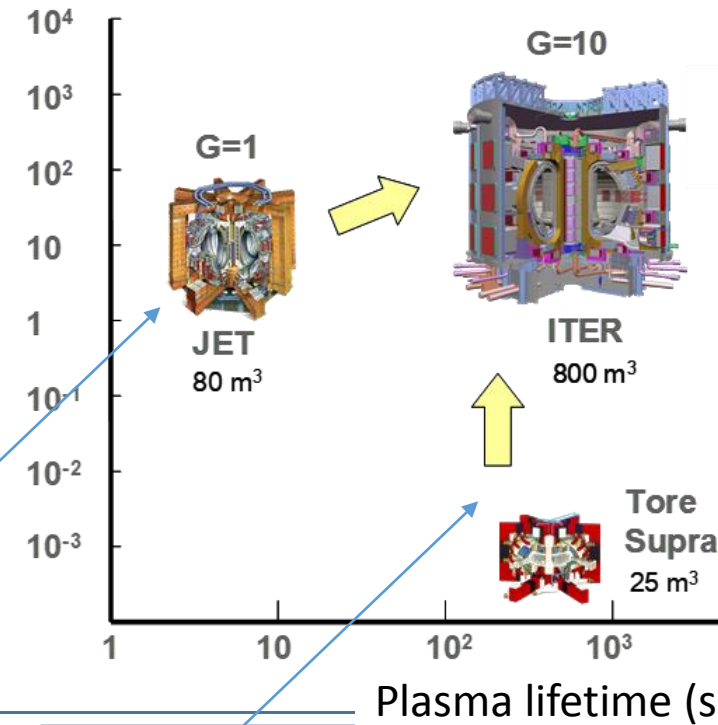


[E.Gauthier SOFT, 2006]



18/05/2021 Jean.-Luc. Leray
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P
(MW_{th})



[D. Guilhem]

Tore Supra,
Superconducting
wire coils

Cadarache near
Marseilles, Fr

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ITER Timeline

- Recents achievements

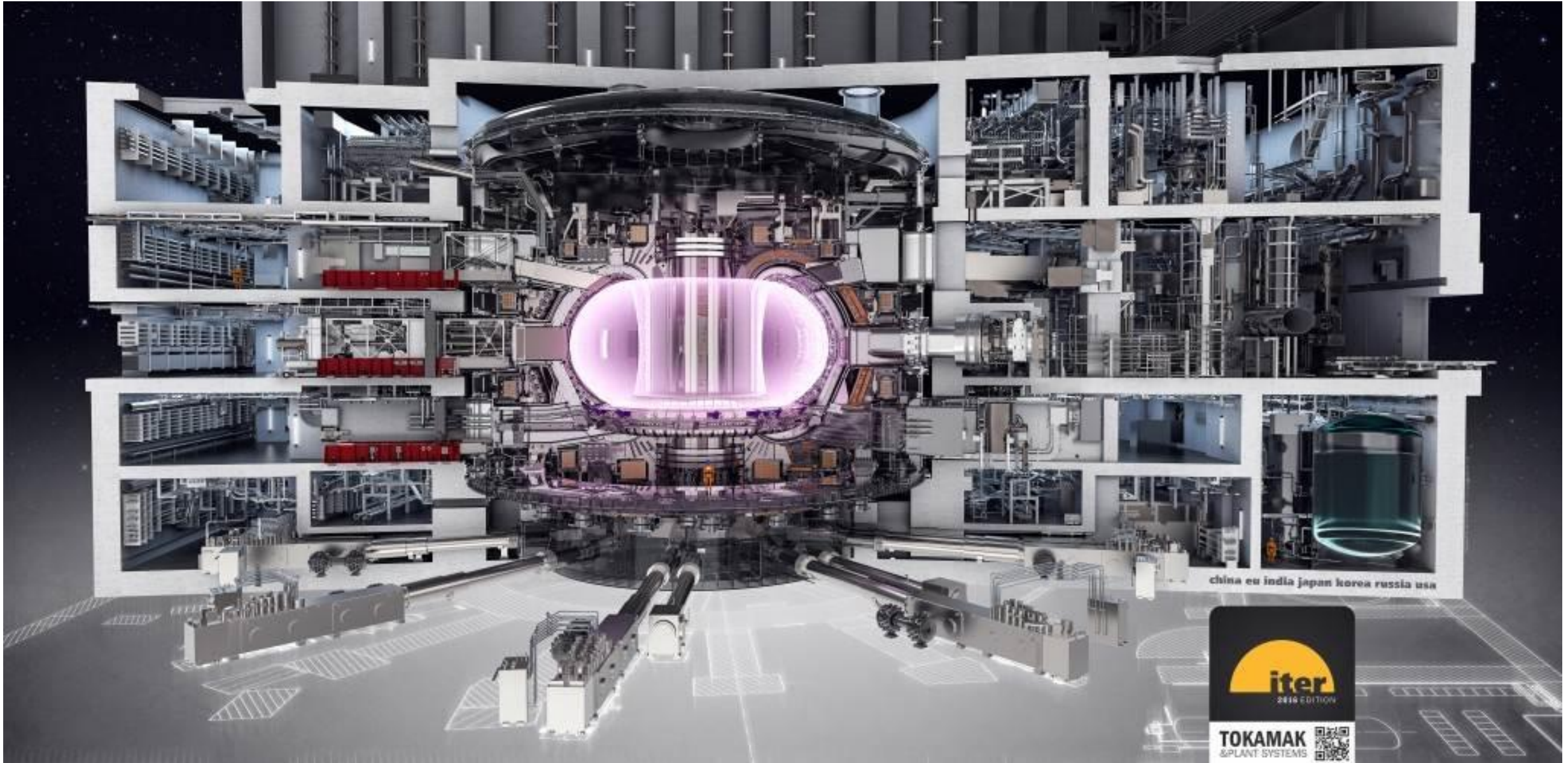
- In November 2017, the project passed the halfway mark to First Plasma.
- In July 2020, the project officially launched the machine assembly phase.
- Today, project execution to First Plasma stands at **71.1 percent** (October 2020 data).

- Future Milestones

- Dec 2025 Commissioning and First Plasma (H2)
- *2025-2035 Progressive ramp-up of the machine*
- *2035 DD-DT Operation begins*

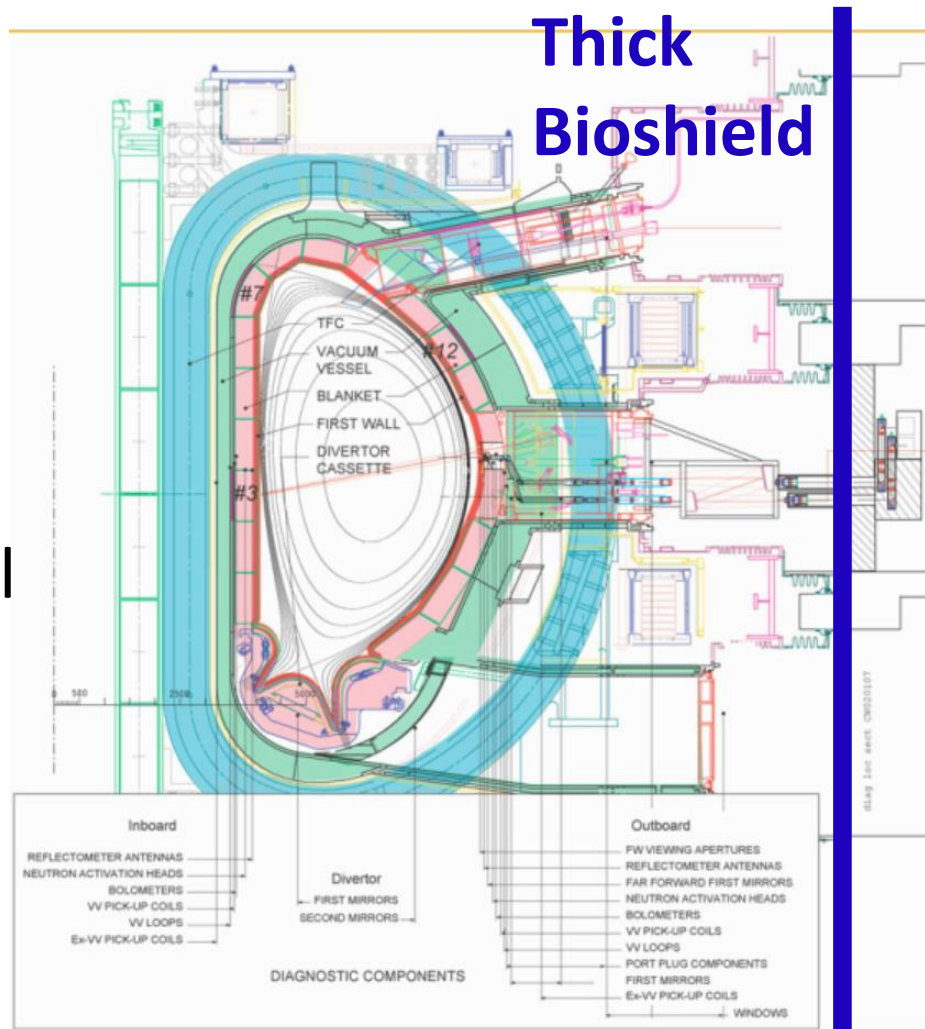
(<https://www.iter.org/proj/inafewlines#6> Dec 6th, 2020)

Tightly packed! The technical areas tied to the Port Cells This design as an example



Generic Sketch

The source region
ie, the plasma
and the 1st wall



Physical
eg, 4 meters diagnostics

Transit of
information to
the outside

ELECTRONICS

Cables, Optical
Fibers...

„Generic diagnostic issues for a burning plasma experiment“, G. Vayakis, E. R. Hodgson, V. Voitsenya, C. I. Walker, Fusion Science and Technology vol. 53 Chapter 12, Feb. 2008, pp 699-750

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TABLE I
KEY ENVIRONMENTAL PARAMETERS FOR JET, ITER, AND CANDIDATE DEMO DESIGNS

Parameter	JET	ITER	DEMO
First Wall neutron flux	$\sim 3 \cdot 10^{13} \text{ n/cm}^2\cdot\text{s}$	$\sim 3 \cdot 10^{14} \text{ n/cm}^2\cdot\text{s}$	$\sim (0,3 \text{ to } 1) \cdot 10^{15} \text{ n/cm}^2\cdot\text{s}$
Plasma volume (m ³)	80	850	900 – 2,700
Pulse length (s)	~ 20	400 - 3000	-
Fusion power (MW)	~ 16 (max)	~ 500	2,500 – 5,000
Total plasma lifetime at high performance (hr)	-	4,700	0(90,000)
Stored thermal energy (MJ)	~ 4	~ 400	1000 - 2000
First wall neutron flux (n/m ² ·s)	3×10^{17} (max)	3×10^{18}	$\sim (3 - 10) \times 10^{18}$
Total neutron source strength (n/s)	1.2×10^{19} (max)	1.4×10^{21}	$1.4 - 7 \times 10^{21}$
Charge exchange wall load (kW/m ²)	~ 0.2	~ 1	-
Neutron load at first wall (MW/m ²)	~ 0.05 (max)	~ 0.5	1-3
Neutron fluence (MWa/m ²)	0(0)	0.3	5 - 15
Neutron fluence (n/m ²)	$\sim 3 \times 10^{21}$	$\sim 3 \times 10^{25}$	$\sim (50 - 150) \times 10^{25}$
Displacement damage at first wall (dpa)	0(0)	~ 3	50 - 150

Alan E. Costley, "Towards Diagnostics for a Fusion Reactor", IEEE Transactions on Plasma Science, Vol. 38, no. 10, October 2010, 2934.

First principles, simple approach, rule of thumb

- 500 MW, 14 MeV

Assumption of a spherical source, isotropic

Fusion neutrons $dn/dt \sim P (W) / 14 \text{ MeV} / (eV) / (eV/W) \sim 2,2 \cdot 10^{20} \text{ n/s}$

Flux at a distance d from the “center” $\Phi_n \sim \frac{1}{4\pi d^2} dn/dt$

$\Phi_n \sim 7 \cdot 10^{13} \text{ n/cm}^2/\text{s}$ at 5m ~Vessel, First Wall ($\Phi_n \sim 2 \cdot 10^{13} \text{ n/cm}^2/\text{s}$ at 10m)

In 4700 hours, the fluence could be some 10^{21} n/cm^2 However, it is not realistic to place Electronics without very thick shielding

Actually, the Bioshield is meters thick to provide sufficient neutron captures, over $1/10^7$ in flux (up to 10^{11} and more according to the location)

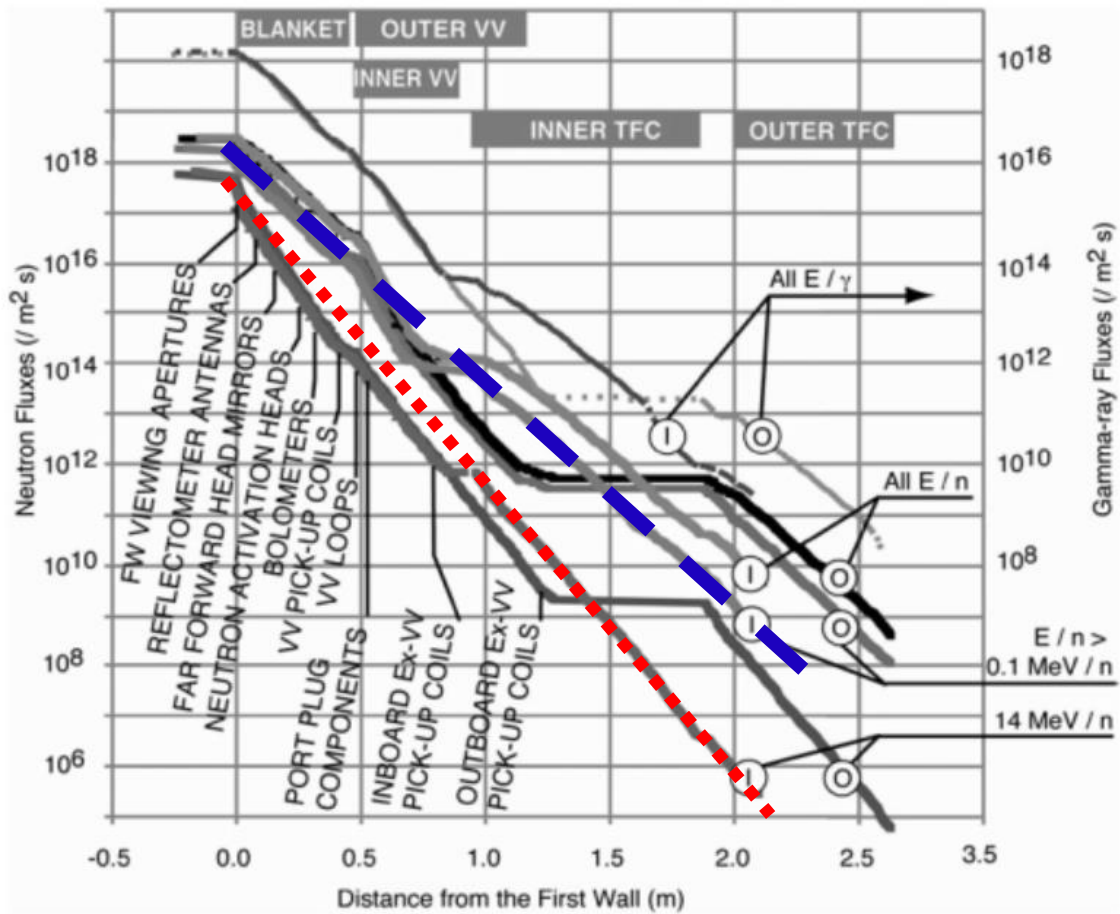
As a result, a number of gamma comes from in the inner part of the machine (tens of thousand tons) => TID

**And, the neutron spectrum suffers reduction by the captures and is softening as well
=> From 2,45 MeV (DD) or 14 MeV (DT) to thermalization, 1/E white spectrum expected,
=> LARGE SEE rate and in places significant DDD.**

Calculation of the neutron spectrum in every location of the area also is an immense problem.

Spectrum softening along the radial axis

Vayakis et al. GENERIC ISSUES FOR BURNING PLASMA EXPERIMENT



- This early calculation in radial model quantitatively shows the enhancement of >100 keV group with respect to the >14 MeV line
- 3 to 4 decades at 2 meters from the 1st Wall
- Consequently, the SEEs are very sensitive on the actual spectrum at the location of use.
- 1/E slowing spectrum is expected at least at lower energies, inside bioshield as well as outside in experimental areas

— — — — — >100 keV
 >14 MeV

Fig. 2. Neutron and gamma fluxes on diagnostic components during operation for 500 MW. The solid curves are from a simplified 1D equivalent (cylindrical) model of the machine. This averages out the effect of gaps and does not include diagnostic penetrations.

„Generic diagnostic issues for a burning plasma experiment“, G. Vayakis, E. R. Hodgson, V. Voitsenya, C. I. Walker, Fusion Science and Technology vol. 53 Chapter 12, Feb. 2008, pp 699-750

COMPARISON WITH FISSION (conceptual for Single Event Effects)

- Inside a water-cooled power Fission Reactor, layout consist of submerged fuel rods. Water scatters and array of rods both are a source and an absorber
- In a Fusion Reactor, the plasma vessel is surrounded by thick absorbers (Li, Water coolant pipes) and thick shield which absorb and scatter.
- Both spectra are governed by a Boltzmann equation

As a result the spectra look rather the same.

In Nuclear Fission engineering, the coarse spectrum is first orderly as this (1) :

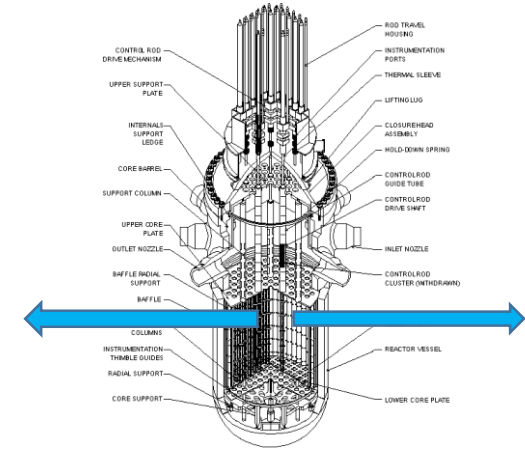
$$\phi_E(E) = \begin{cases} C_1 \frac{E}{(kT)^2} e^{-\frac{E}{kT}} & \text{if } E < E_{\text{thermal}} \\ 1/E & \text{if } E_{\text{thermal}} < E < E_{\text{fast}} \\ C_2 \chi(E) & \text{if } E > E_{\text{fast}} \end{cases}$$

With $E_{\text{thermal}} = 0,5 \text{ eV}$ and $E_{\text{fast}} = 0,5 \text{ MeV}$

The shape of $\chi(E)$ is determined by the source and the heavy materials, absorption and density

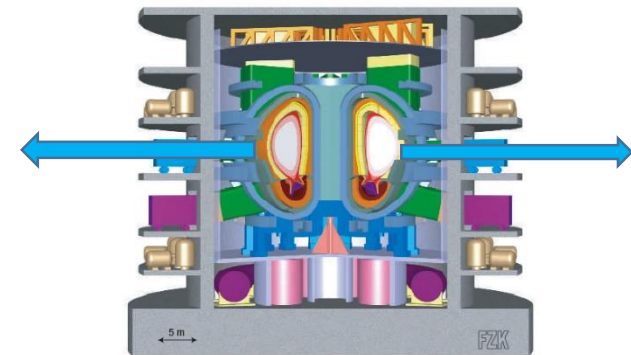
Source = fission spectrum or damped fusion line (14 MeV)

Fission Reactor (PWR) with its Assemblies



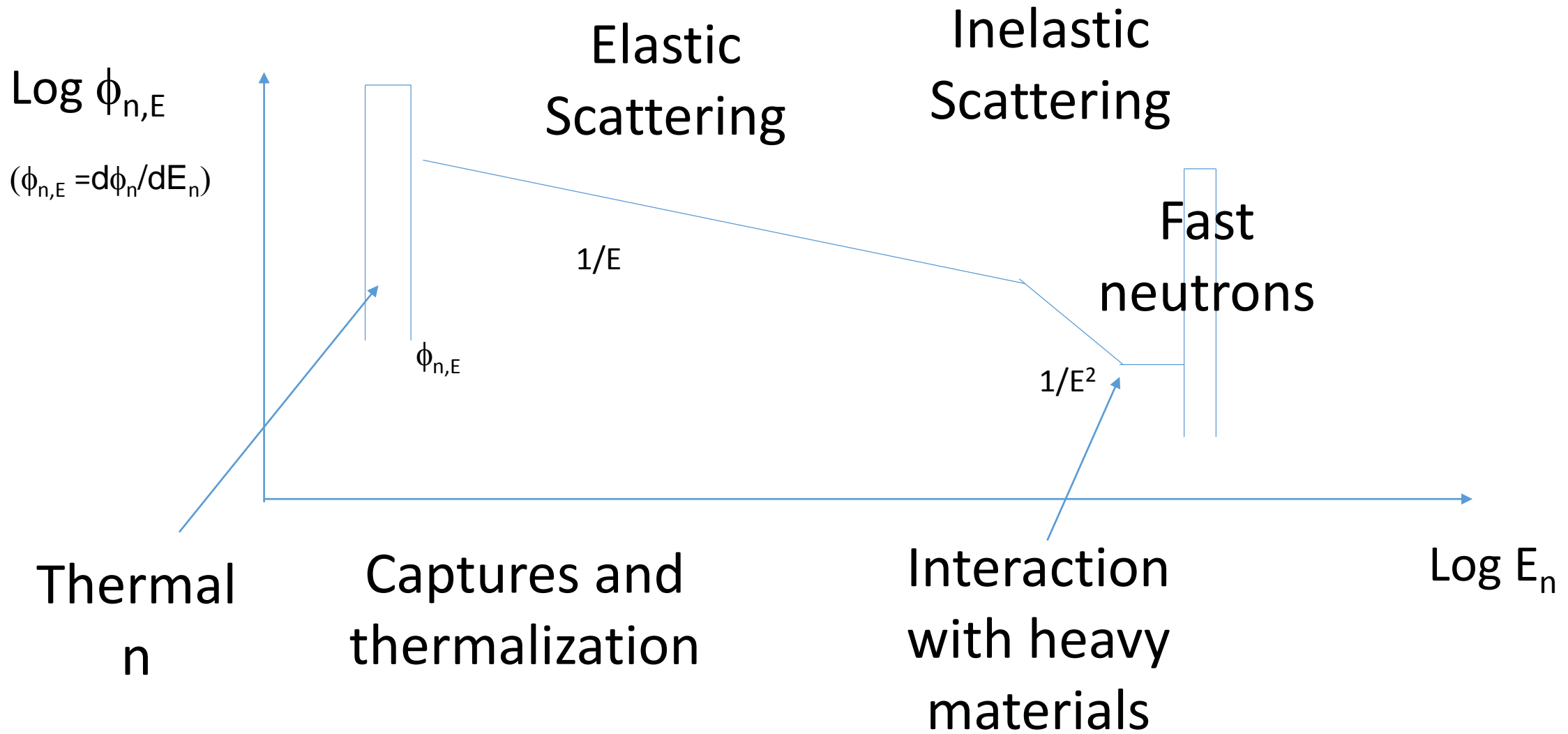
Residual neutron Flux outside the pressurized Vessel, inside the Bldg

Fusion Power Reactor with its Shields

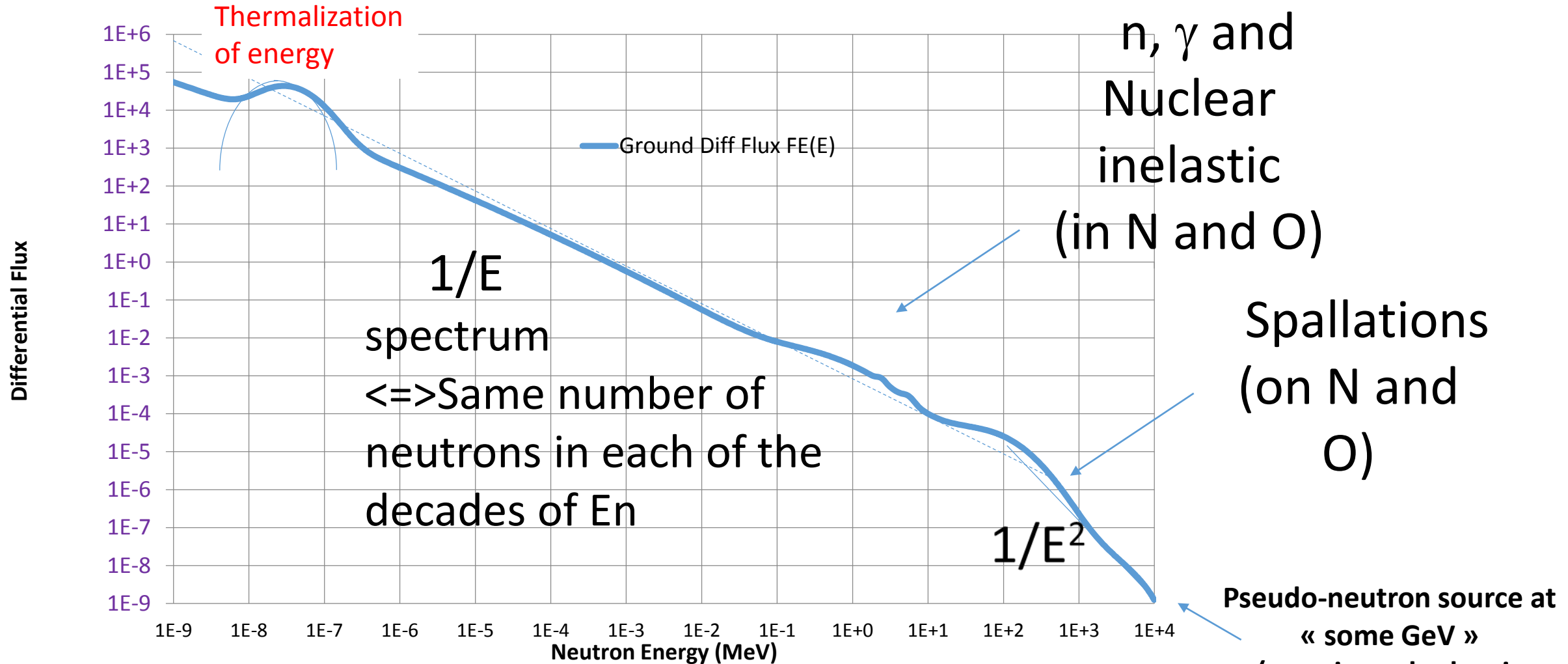


Residual neutron Flux outside the Shield In the technical front areas

Modeling the spectrum in broad (coarse) regions (Fusion) Varies with shields design



Comparison with a typical natural neutron spectrum in the atmosphere, at ground level



in "SOFT ERRORS", in Jean-Luc Autran and Daniela Munteanu (fig 1.12 p. 20) and M.S. Gordon, P.Goldhagen et Al, IEEE tTNS TNS-51

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Shape of the SEU Modeling (Monte Carlo) by IM2NP, Aix-Marseille University

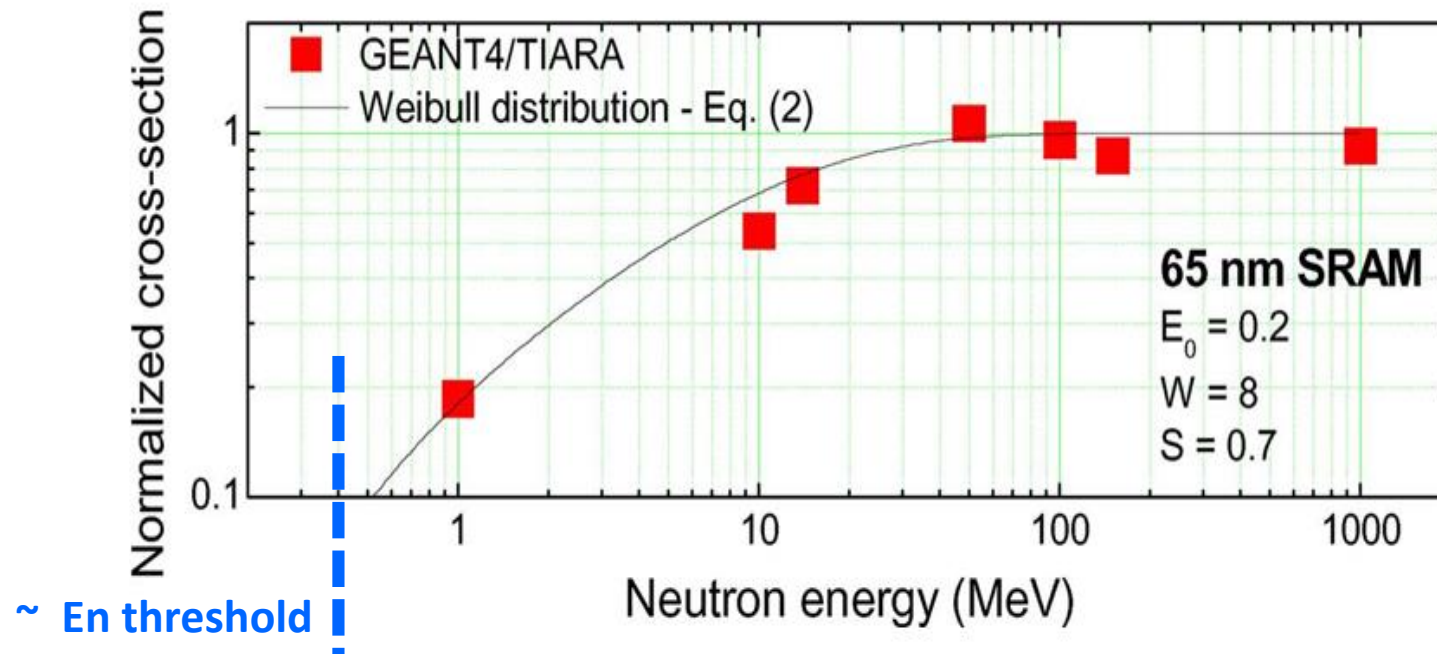
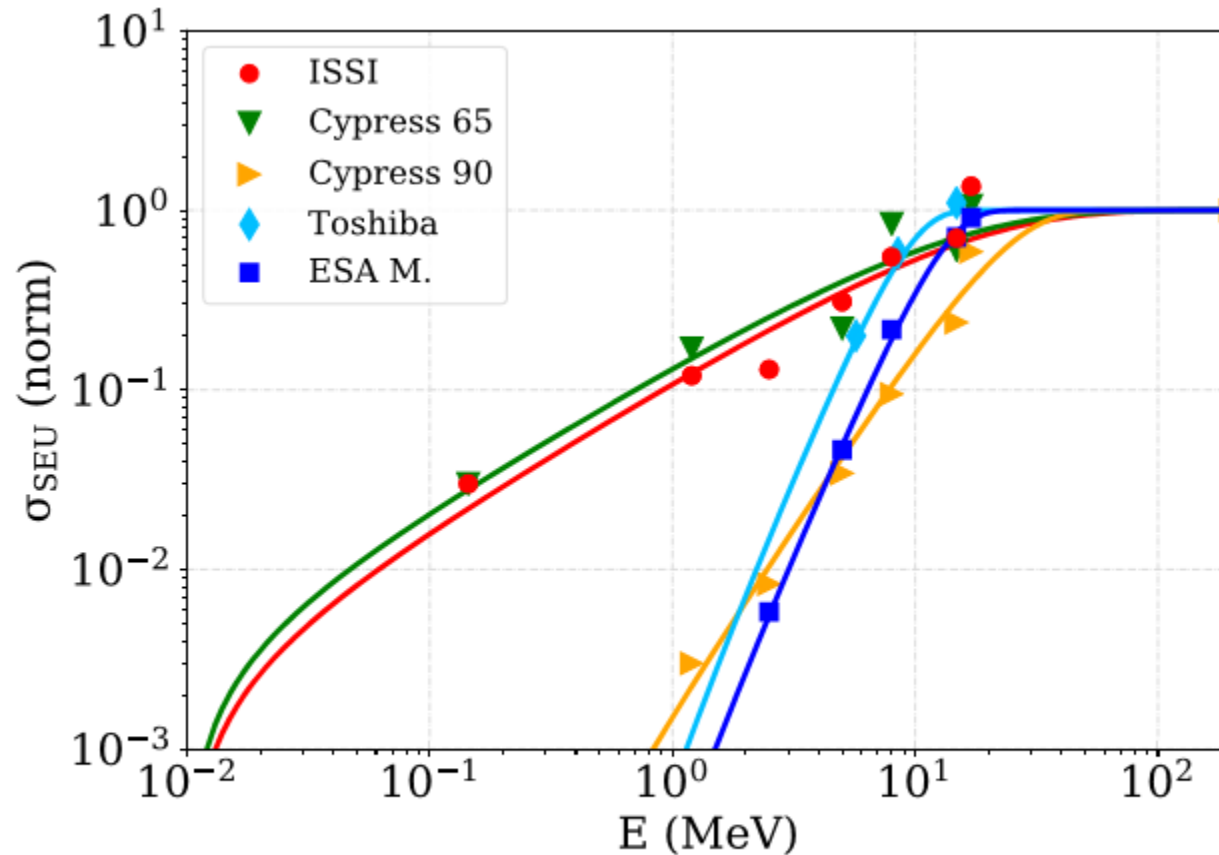


Fig. 8. TIARA values and normalized Weibull fitting (using (2)) of the 65 nm SRAM cross-section.

„Soft Errors, from particles to circuits”, Jean-Luc Autran and Daniela Munteanu, CRC Press, 2015

Matteo Cecchetto's Thesis and publications (Apr 2021)



(b)

Matteo Cecchetto, Experimental and simulation study of neutron - induced Single Event Effects in accelerator environment and implications on qualification approach, CERN & ISE-Montpellier Univ., PhD Thesis April 2021, p.145

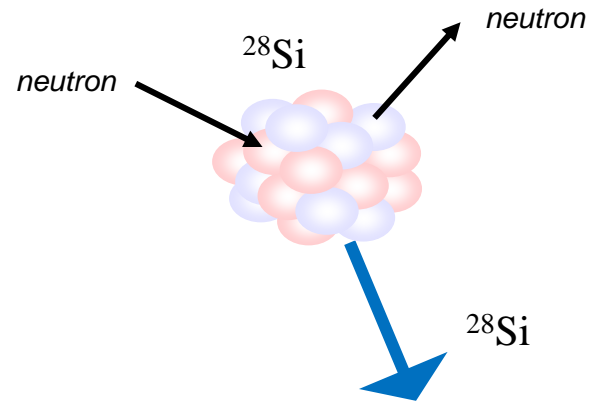
Table 7.5: Weibull fit parameters of the tested memories and those of the Toshiba reference (from [10]) for the HEHeq calculation.

Memory	σ_{sat} [cm ² /bit]	E_{th} [MeV]	W [MeV]	s
ISSI 40 nm	$1.40 \cdot 10^{-14}$	0.01	14.05	0.82
Cypress 65 nm	$7.73 \cdot 10^{-14}$	0.01	11.57	0.80
Cypress 90 nm	$2.16 \cdot 10^{-13}$	0.1	24.22	1.98
ESA M. 250 nm	$2.60 \cdot 10^{-14}$	0.2	13.08	2.99
Toshiba 400 nm	$6.60 \cdot 10^{-14}$	0.2	9.25	3.02

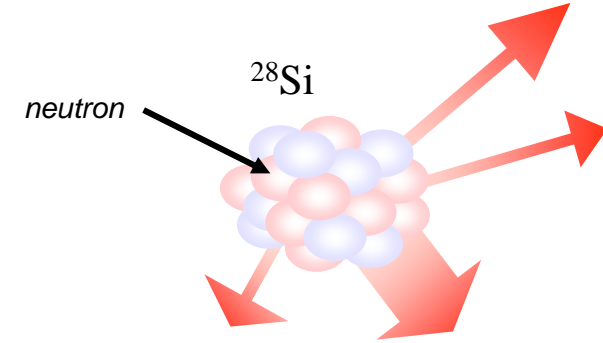
Back to the nuclear interaction: example of neutron in silicon

Capture, quasi fission, or scattering

- Neutron scattering, silicon recoil



- Exothermic nuclear silicon break-up



- No threshold
- Cross section

By-products (recoils) n energy thresholds cross section

$^{25}\text{Mg} + \alpha$ 2.75 MeV

$^{28}\text{Al} + p$ 4.00 MeV

$^{27}\text{Al} + d$ 9.70 MeV

$^{24}\text{Mg} + n + \alpha$ 10.34 MeV

$^{27}\text{Al} + n + p$ 12.00 MeV

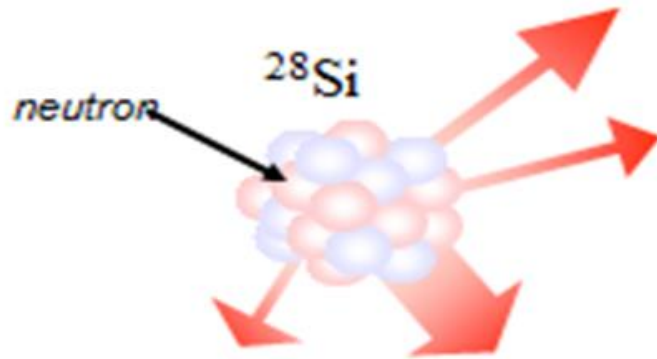
$^{26}\text{Mg} + ^3\text{He}$ 12.58 MeV

$^{21}\text{Ne} + 2\alpha$ 12.99 MeV

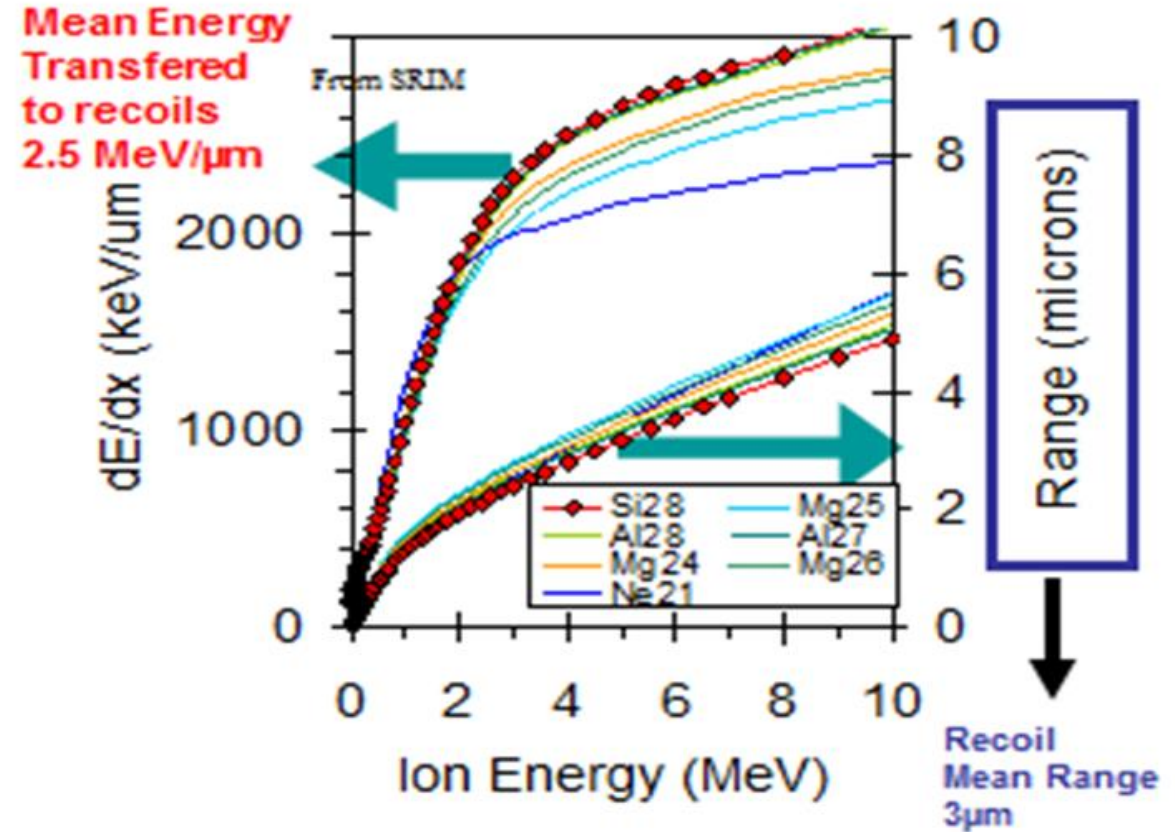
Sketch from Robert Baumann Short
Course, RADECS 2001

What effects of one neutron in silicon?

Neutron => Silicon Recoil Range = 10µm



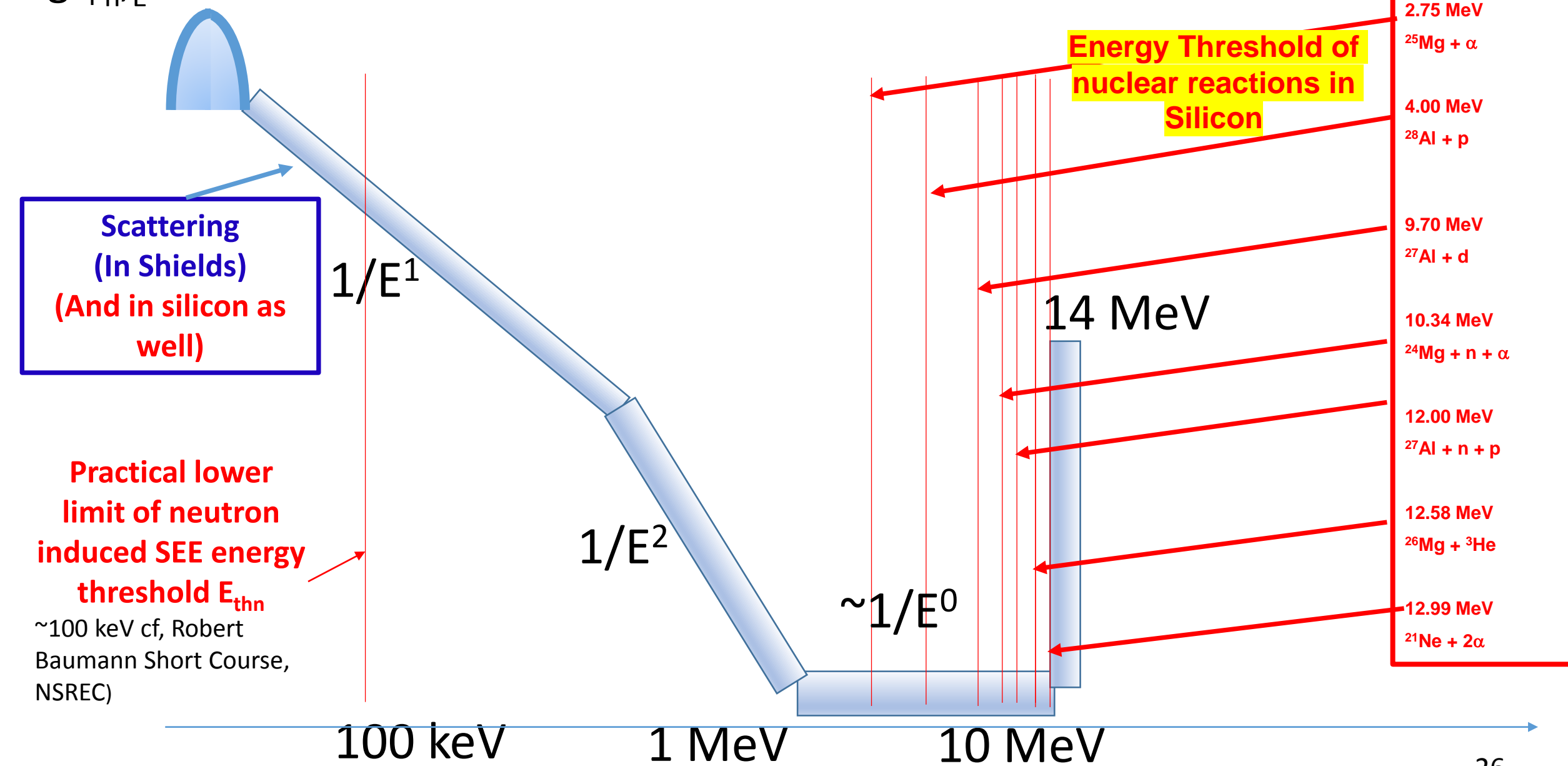
Products	Thresholds
$^{24}\text{Mg} + \alpha$	2.75 MeV
$^{26}\text{Al} + p$	4.00 MeV
$^{27}\text{Al} + d$	9.70 MeV
$^{24}\text{Mg} + n + \alpha$	10.34 MeV
$^{27}\text{Al} + n + p$	12.00 MeV
$^{26}\text{Mg} + ^2\text{He}$	12.58 MeV
$^{21}\text{Ne} + 2\alpha$	12.99 MeV



Sketch from Robert Baumann Short Course, RADECS 2000
 Robert Baumann, Wrobel et al., IEEE Trans. Nucl. Phys., Vol. 47, No. 5, Dec. 2000

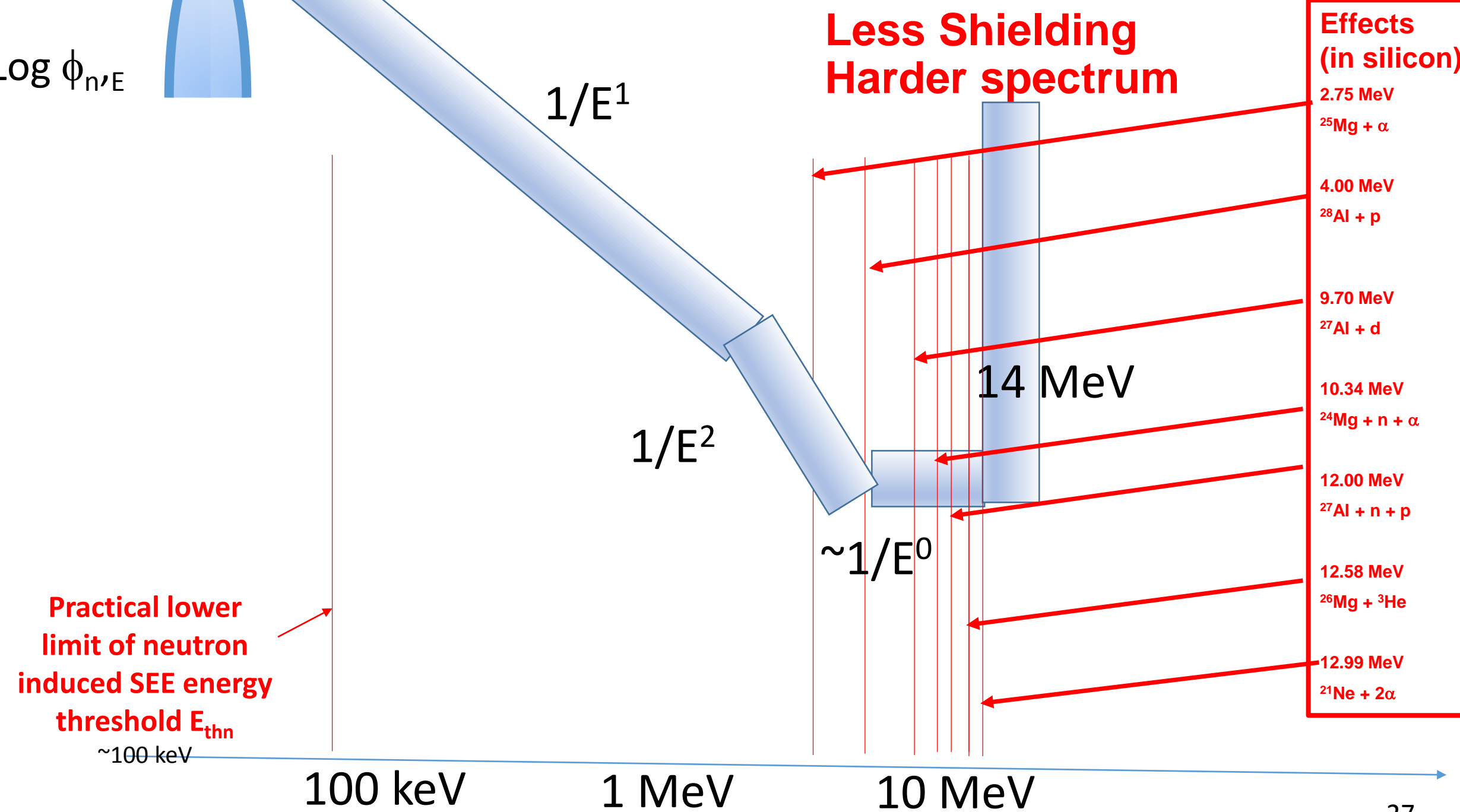
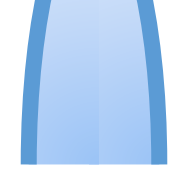
**Need for of a simple parametrizable neutron spectrum
for use by radiation electronics engineers and researchers for testing**

Log $\phi_{n,E}$



Practical lower limit of neutron induced SEE energy threshold E_{thn}
 ~100 keV cf, Robert Baumann Short Course, NSREC)

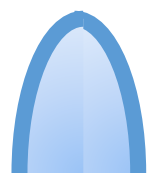
Log $\phi_{n,E}$



Log $\phi_{n,E}$

**More Shielding
Softer spectrum**

**Effects
(in silicon)**



$1/E^1$

$1/E^2$

14 MeV

$\sim 1/E^0$

**Practical lower
limit of neutron
induced SEE energy
threshold E_{thn}
~100 keV**

- 2.75 MeV
 $^{25}\text{Mg} + \alpha$
- 4.00 MeV
 $^{28}\text{Al} + p$
- 9.70 MeV
 $^{27}\text{Al} + d$
- 10.34 MeV
 $^{24}\text{Mg} + n + \alpha$
- 12.00 MeV
 $^{27}\text{Al} + n + p$
- 12.58 MeV
 $^{26}\text{Mg} + ^3\text{He}$
- 12.99 MeV
 $^{21}\text{Ne} + 2\alpha$

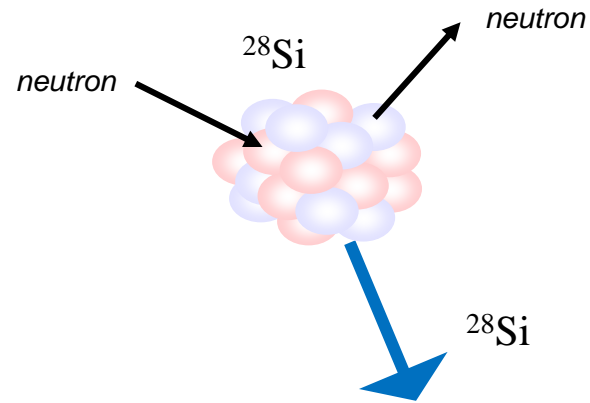
100 keV

1 MeV

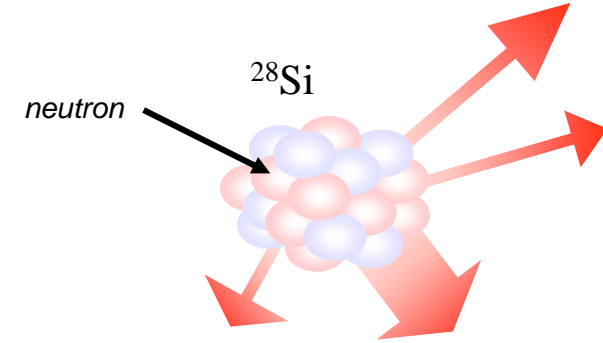
10 MeV

Back to the nuclear interaction: One neutron in silicon

- Neutron scattering, silicon recoil



- Exothermic nuclear silicon break-up



- No threshold
- Cross section

By-products (recoils) n energy thresholds cross section

$^{25}\text{Mg} + \alpha$ 2.75 MeV

$^{28}\text{Al} + p$ 4.00 MeV

$^{27}\text{Al} + d$ 9.70 MeV

$^{24}\text{Mg} + n + \alpha$ 10.34 MeV

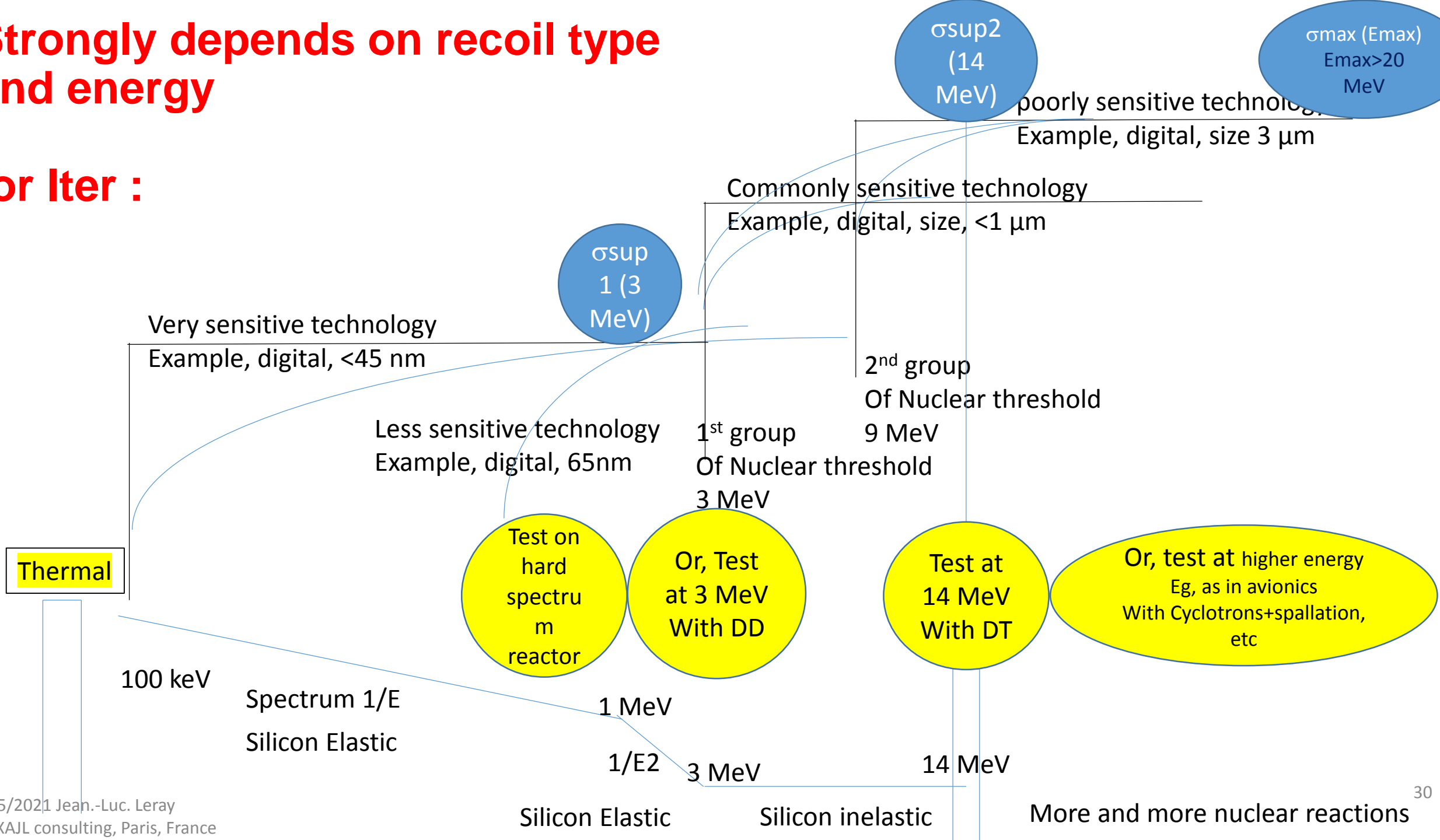
$^{27}\text{Al} + n + p$ 12.00 MeV

$^{26}\text{Mg} + ^3\text{He}$ 12.58 MeV

$^{21}\text{Ne} + 2\alpha$ 12.99 MeV

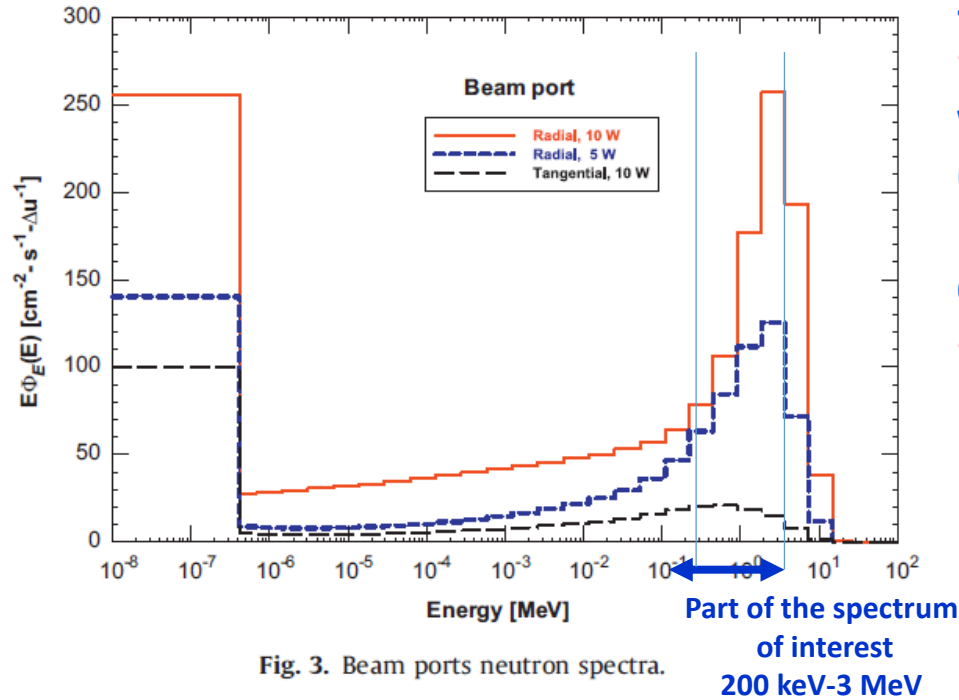
Strongly depends on recoil type and energy

for Iiter :



Test at higher flux or larger beam for PCB

Example of a Triga fission reactor
(neutron 3 MeV-peaked latency spectrum)



Suited for

- Bin B3a = 200 keV – 3 MeV with filters to block below 1 keV (100 keV...?)

Optionally suited for

- Bin B1 = thermal if such a line exists at the same location : with classical thermalizer and filters and spectrum characterization + dosimetry

H.R. Vega-Carrillo et al. / Applied Radiation and Isotopes 83 (2014) 252–255, Elsevier National Institute of Nuclear Research in Mexico

Table 1

Integral features of neutrons at the TRIGA Mark III beam ports.

Beam port	ϕ [cm ⁻² s ⁻¹]	E_{Av} [MeV]	$H(10)$ [μ Sv h ⁻¹]
Radial, 5 W	1073 ± 63	0.6906	505 ± 30
Radial, 10 W	2085 ± 122	0.8166	934 ± 55
Tangential, 10 W	537 ± 31	0.1853	106 ± 6

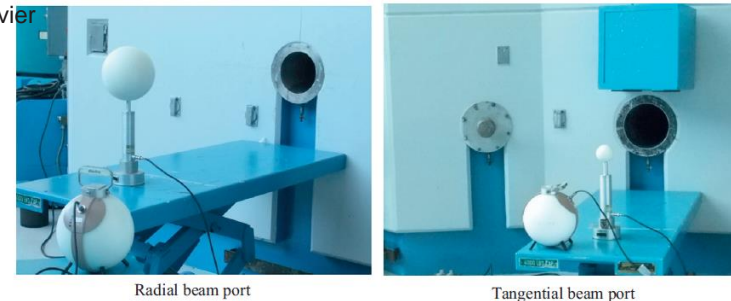


Fig. 1. TRIGA Mark III beam ports.

SEE TEST PROCEDURE
for the Iiter-specific neutron radiation

ITER-CERN
RHE WORKSHOP
23/MAY/2018

SUMMARY on RADIATION (neutron)

• Unmitigated

- The neutron flux is expected to a very high ceiling near the Vessel
- Thanks to the cooling system and very efficient bioshield, the radiation levels are expected to decrease significantly as one moves further away.

• Mitigation

- In some places the electronics can be forbidden.
- However, for non-critical applications, the use of Commercial-Off-The-Shelf components and modules is foreseen.
- Electronics is likely to be relocated outside as much as possible

- **TESTING TO NEUTRON MUST TAKE EXTREME CARE OF THE SPECTRUM :
the one at the proper location and the one of the TEST MACHINE**
- **COMPLIANCE RULES MUST BE SET TO ALLOW COMPLIANCE OF THE
TEST SPECTRUM WITH THE DESTINATION NEUTRON SPECTRUM**

Similarities and differences in TESTING between Avionics and Fusion

(Similarities: 1/E spectrum down to thermal energy)

avionics

- Apparent Neutron source is at « some GeV »
- Testing
- **JEDEC/JESD89 standard is the reference for testing devices**
- High Energy Test is recommended between 10 MeV and 1 GeV
- The opinion of JESD89 members (IEEE/NSREC Conference 2018) is that the component of Single Event Rate below 10 MeV is of minor interest
 - Because there are few neutrons compared to neutrons above 10 MeV)
- Test at high energy
 - Either using a naturel spectrum on mountains
 - Or a spallation spectrum (cyclotrons), and/or p+ at higher energy
 - Or a synthetic formula of 4 monoenergetic tests between 10 and 100 MeV and 14 MeV n

fusion

- Neutron source energy is at 14.1 MeV or 2,45 MeV
- Testing
 - Specific method between 14 MeV down the thermal energy
 - With suitable sources
 - But such sources are not easily adjustable in energy

Thank you for your attention

We have

- Described spectrum-specific issues in fusion
- Compared with the Atmospheric neutron case (avionics)
- Proposed testing method bases on three neutron energy lines , thermal, 3 MeV, 14 MeV
- Provided caveats for other neutron sources use and method for estimating the SER boundaries

Remarks?
Suggestions?

BACK-UP SLIDES

Year	2001	2004	2007	2010	2013	2016
Litho CD (nm)	130	90	65	45	32	22
Supply Voltage (V)	1.3	1.0	0.7	0.6	0.5	0.4
Nodal Capacitance (fF)	2.00	1.38	1.00	0.69	0.49	0.34
Nodal Charge (fC)	2.60	1.38	0.70	0.42	0.25	0.14
Nodal Charge (electrons)	16250	8654	4375	2596	1538	846

Lawson criteria for the onset of fusion

rate of fusion energy produced by the plasma - loss

- Fusion rate = Number density of fuel A × Number density of fuel B × Cross section(Temperature) × Energy per reaction
- Net power = Efficiency × (Fusion – Radiation loss – Conduction loss)
- The Lawson criterion requires that fusion heating exceeds the losses
figure of merit used by today's fusion scientists, the triple product, to get an energy gain >1.



In 1955, John D. Lawson (4 April 1923-15 January 2008) demonstrated that the conditions for fusion reactions relied on three vital quantities: temperature (T), density (n) and confinement time (τ).

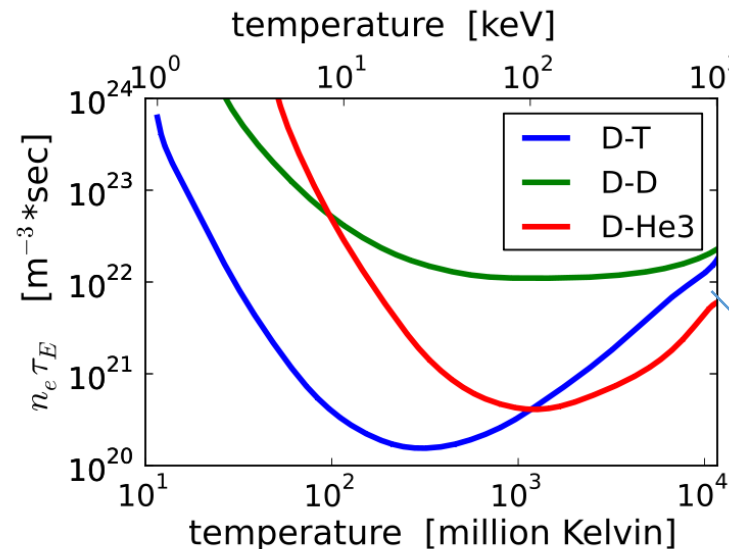
$$n \tau = f(T) \approx \geq 10^{20} \text{ m}^3\text{s}$$

(n density, τ lifetime, temperature)

τ is linked to the nuclear fusion cross section and to the temperature

Inertial
 $n > 200 \text{ gram/cm}^3$
 $\tau < 0.1 \text{ nanosecond}$

https://en.wikipedia.org/wiki/Lawson_criterion



For D-T, the minimum of the product occurs near $200 \cdot 10^6 \text{ K}$ (20 keV)
 Minimum minimum is 30 million degrees (2.6 keV)

Magnetic
 $n > 1 \text{ gram/dm}^3$ (1 bar and > 1 Tesla)
 $\tau > 1 \text{ second} \dots 1000 \text{ second} ?$